

Procjena seizmickog rizika od potresa u urbanim sredinama

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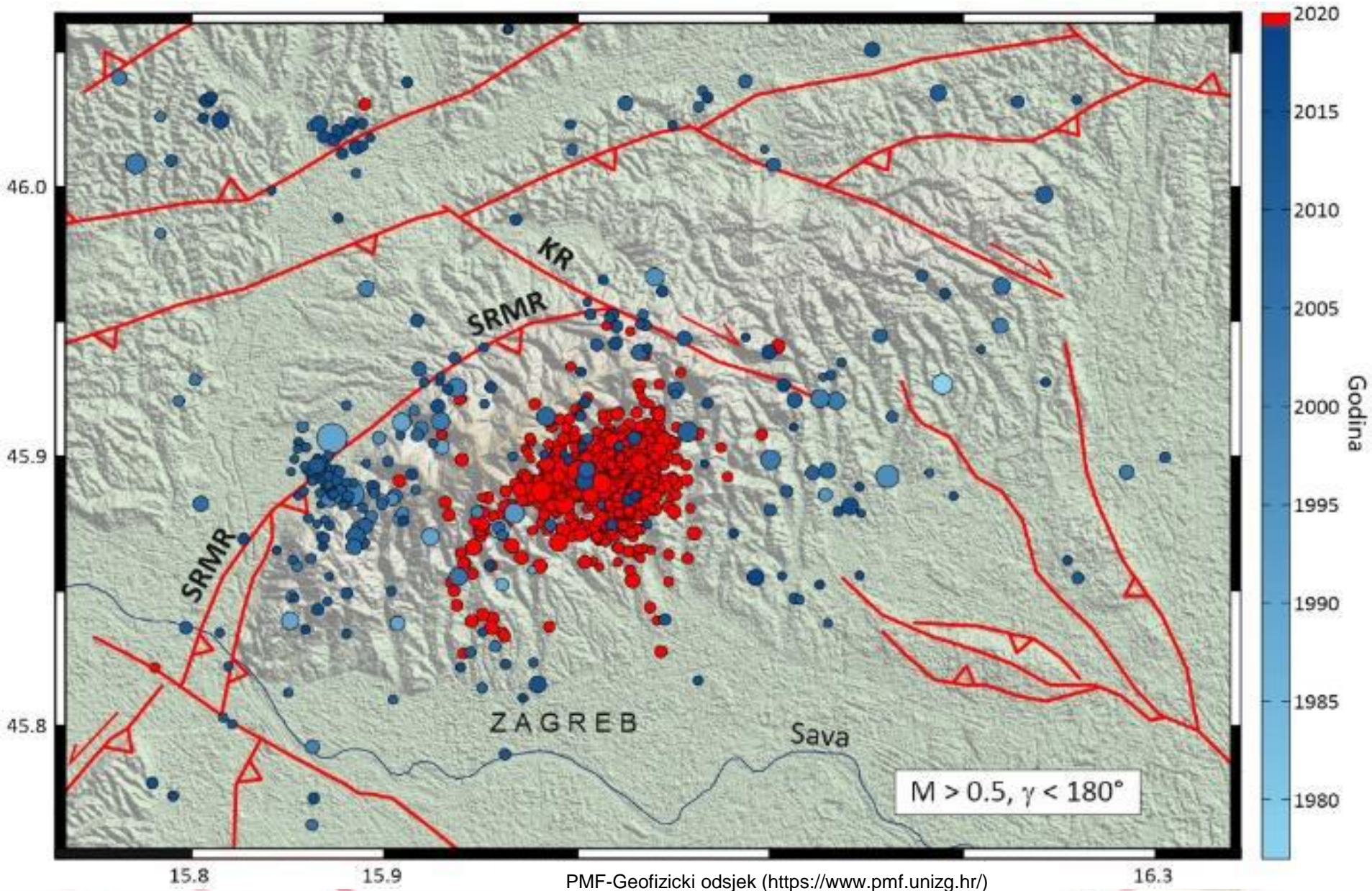
Sveučilište u Zagrebu - Građevinski fakultet, Zagreb, 22 Rujna 2020

Presentation outline

- **Risk assessment process**
- Seismic hazard
- Exposure (izloženost)
- Vulnerability (oštetljivost)
- Risk communication - ER2 Rapid Risk Evaluator



Potresi



Zagrebacki potres



Centar civilne zaštite, Ottawa (CND)



Procjena negativnih utjecaja od potresa



a) Dugoročno planiranje ublažavanja rizika

Interaktivne simulacije “what-if”
scenarios



b) Upravljanje u hitnim situacijama

Procjena negativnih utjecaja u “real
time”



Proces procjene rizika

Hazard

*

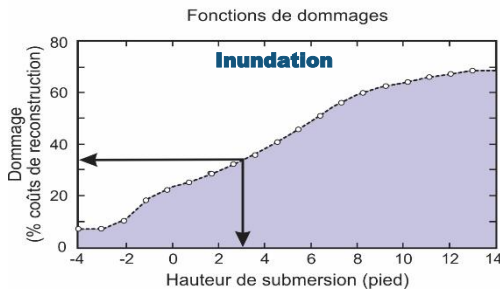
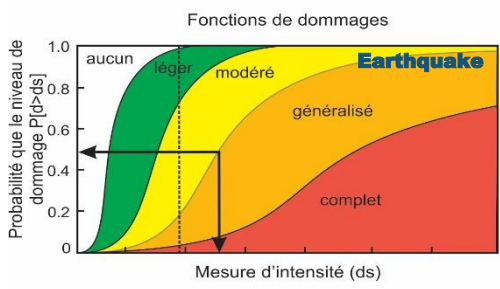
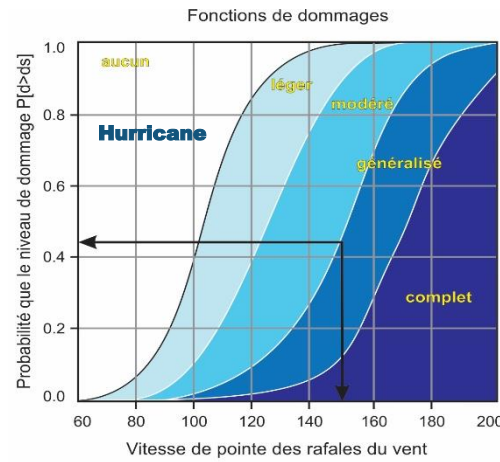
Izloženost

*

Oštetljivost

=

Negativne posljedice



Stakeholders and end-users

- Decision makers for disaster prevention and emergency response
- Land use and urban planners
- Stakeholders who should know about risks
- Authorities who implement costly measures
- Citizens who need relevant information for choosing what to do

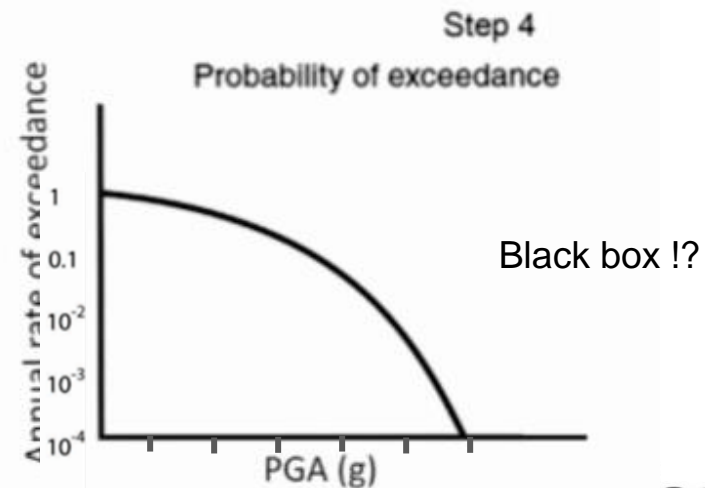
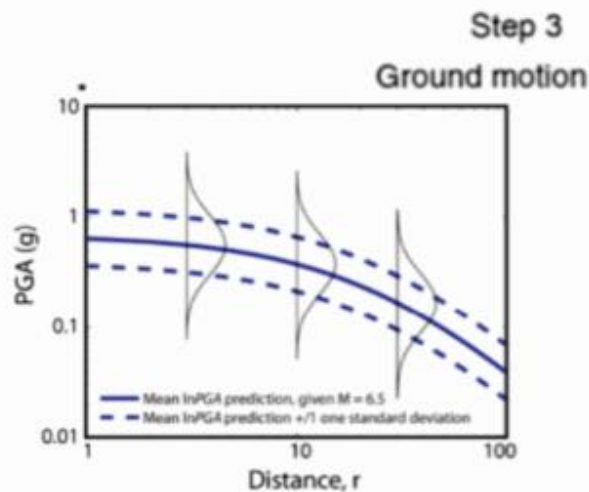
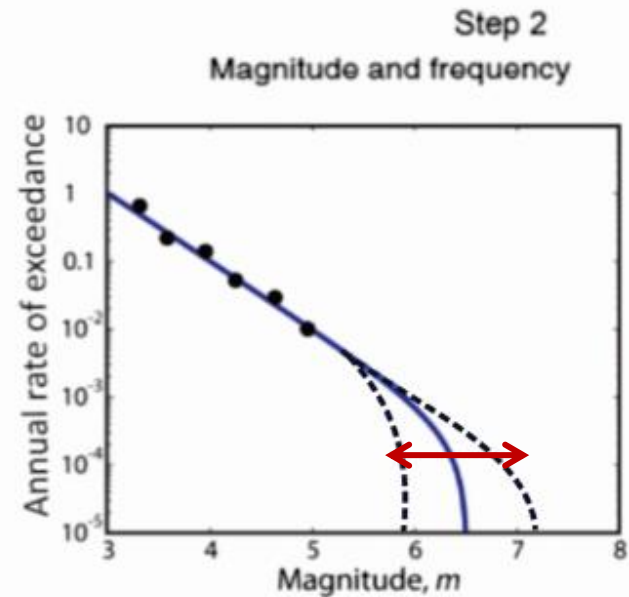
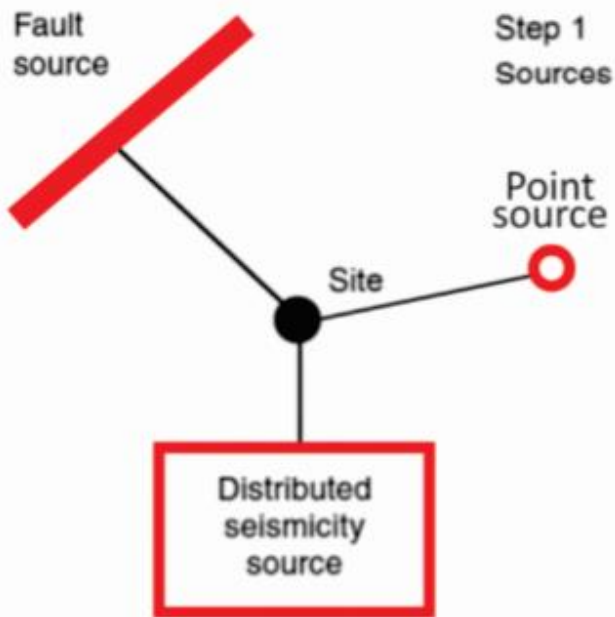


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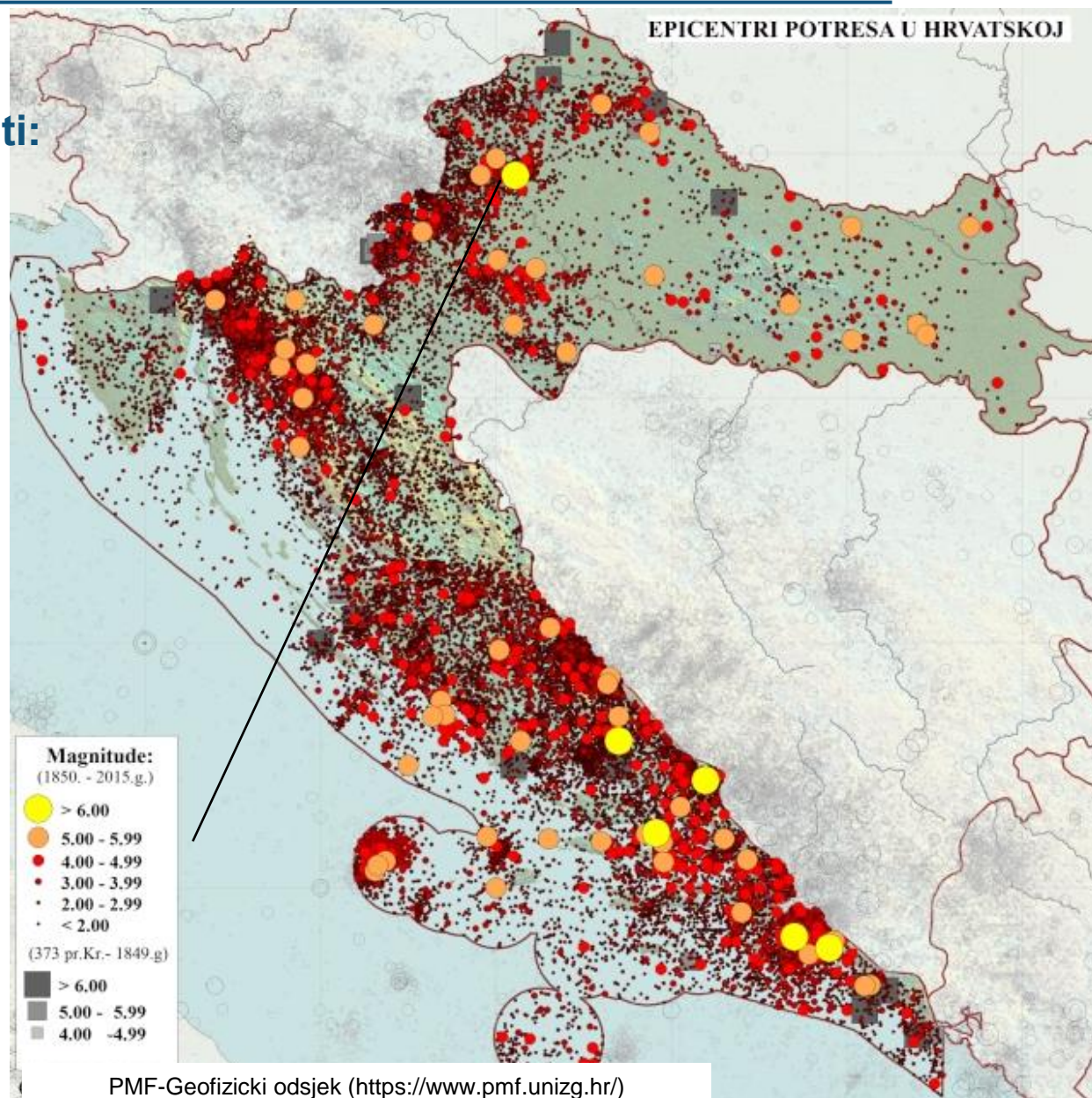
Probabilistic seismic hazard analysis PSHA



Probabilistic seismic hazard analysis PSHA

Hrvatski katalog seizmičnosti:

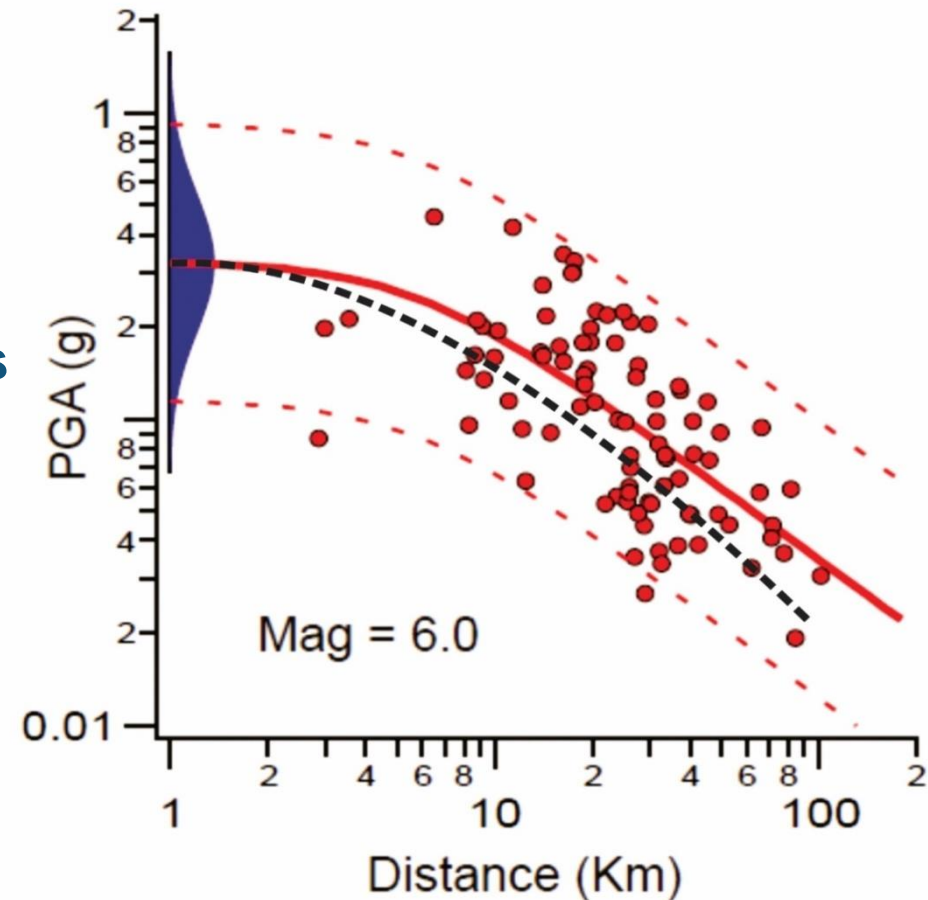
- lokacija,
- jacina, i
- frekvencija potresa



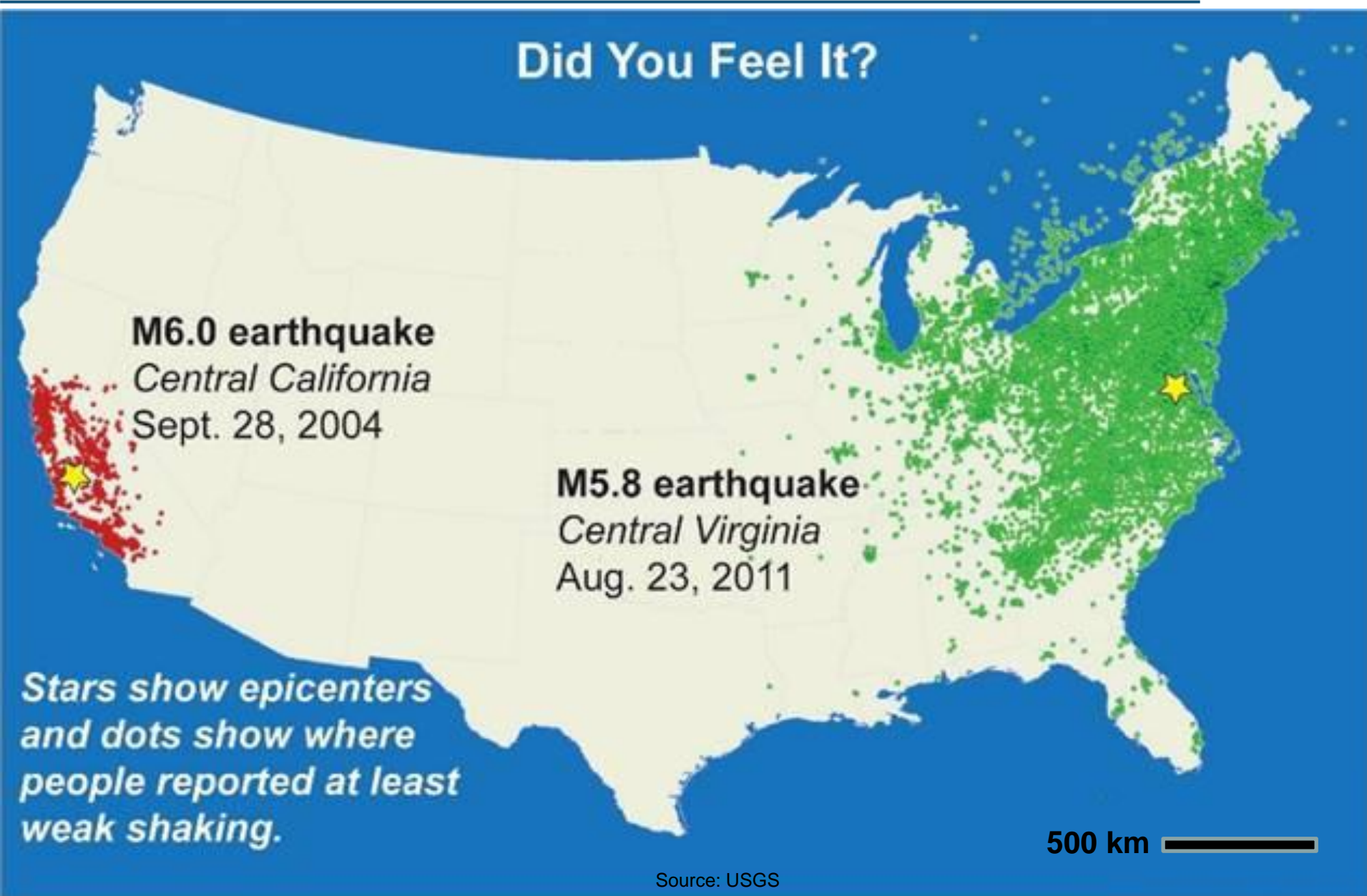
Probabilistic seismic hazard analysis PSHA

GMPEs are developed from strong motion data sets; describe the change of amplitude of seismic shaking with D for given M magnitude.

- regression analysis
- considers inter-event and intra-event variability
- may consider local site conditions
- may consider fault type (n , r , ss)
- estimates mean and σ of PGA, PGV & Spectral accelerations



Probabilistic seismic hazard analysis PSHA



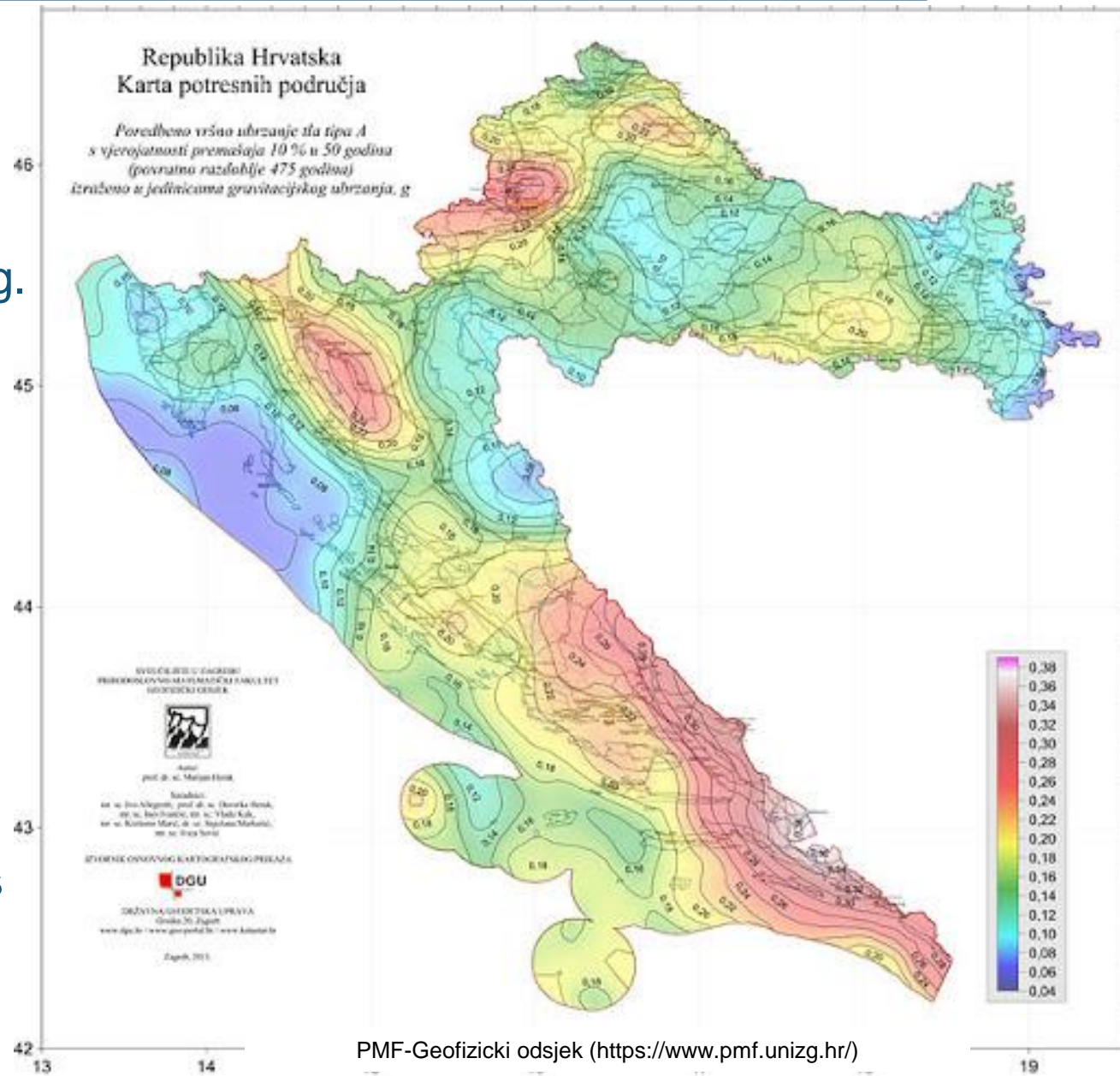
Probabilistic seismic hazard analysis PSHA

Karta horizontalnih vršnih ubrzanja:

- PGA (g)
- Site class A
- Return period of 475g. (10% probability of exceedance in 50yrs vs. 2% in 50 yrs)

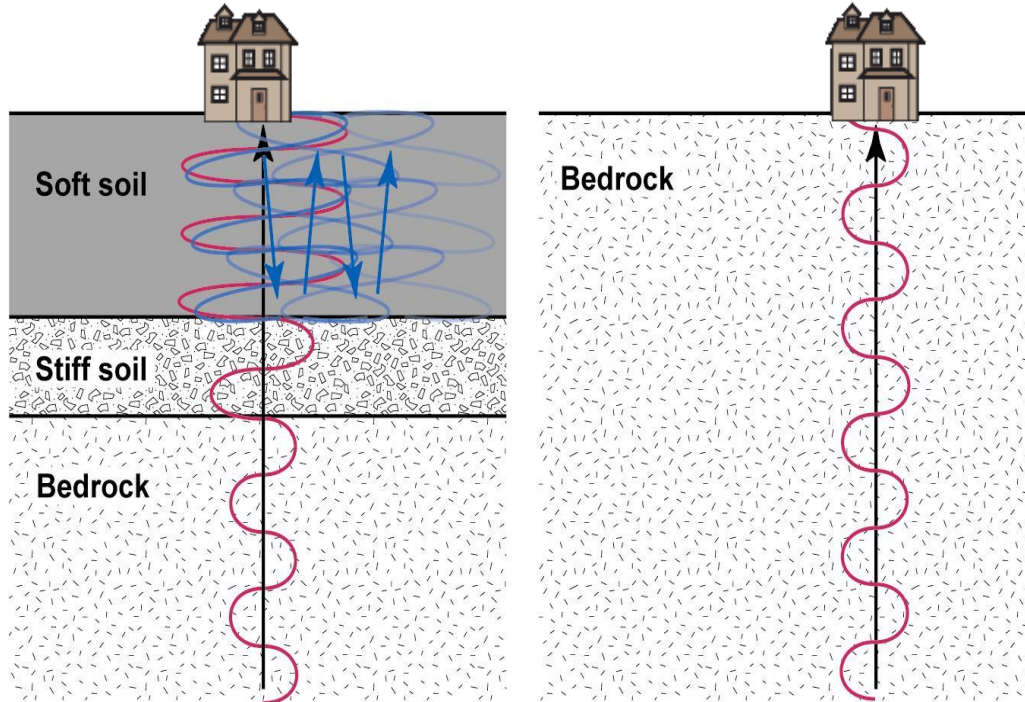
Utility of those maps:

- Engineers
- Insurance industries
- Policymakers & Legislators
- Land-use planners
- Comparisons regions and hazards
- Cost-benefit

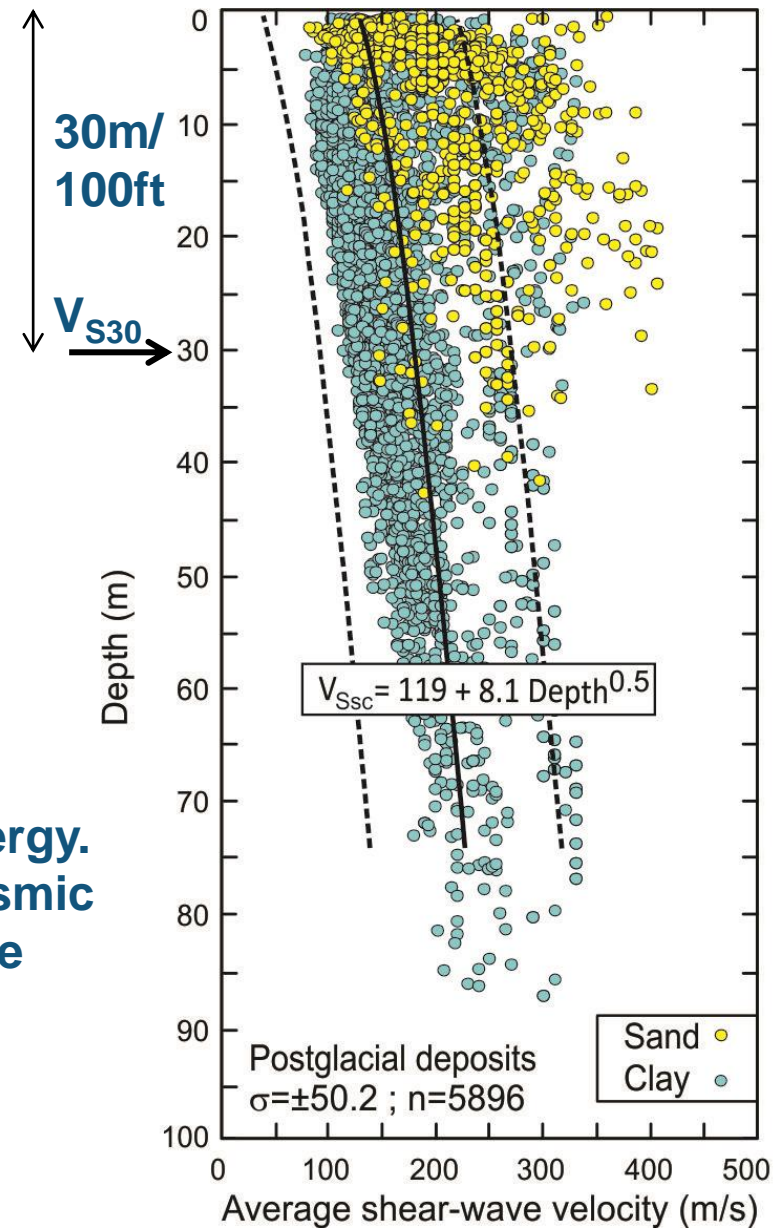


Local site effects

Utjecaj lokalnih uvjeta tla

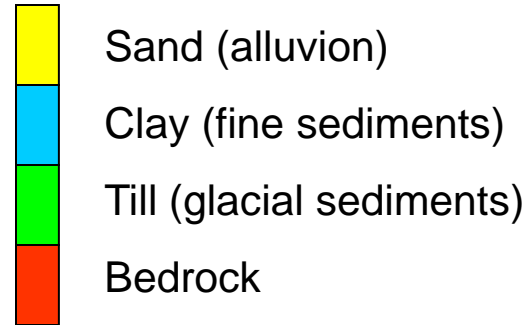
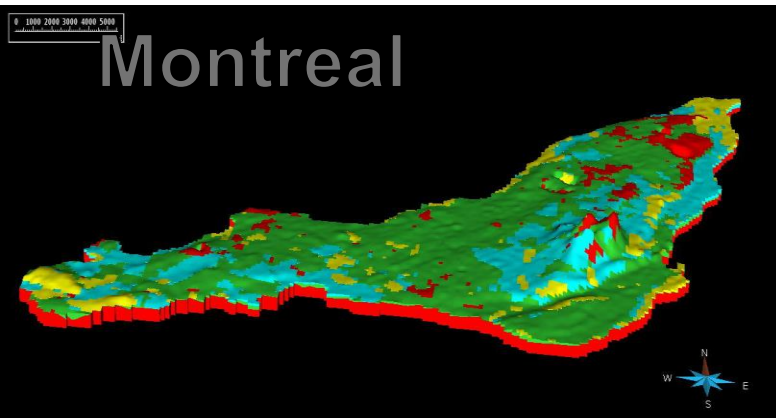


- Seismic waves carry a specific amount of energy. When a lower V_S medium is encountered, seismic waves slow down. To conserve the energy, the amplitude of the seismic waves increases.
- Average vs. Interval V_S

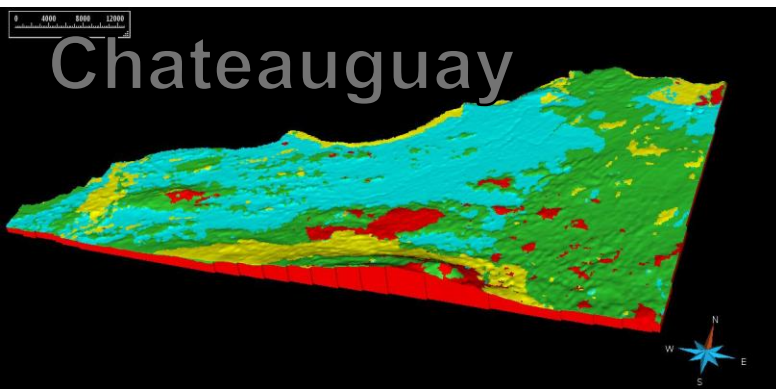


3D Geological models

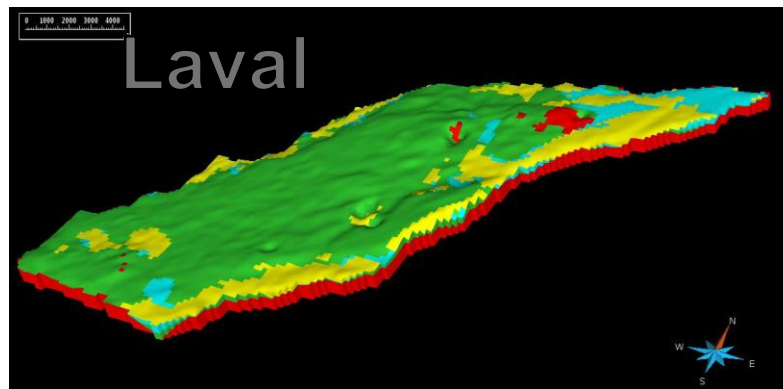
Montreal



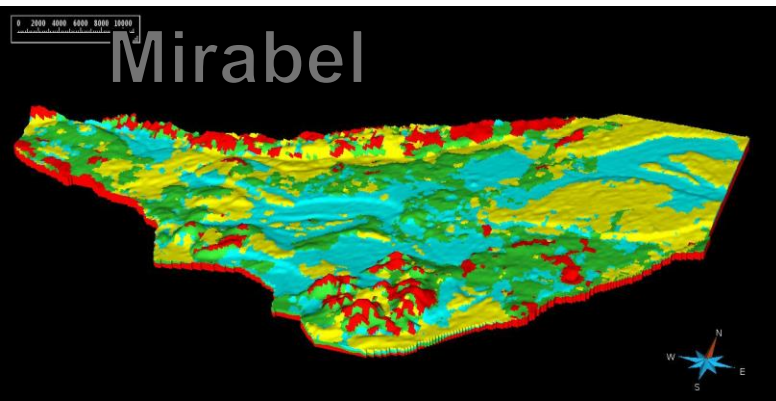
Chateauguay



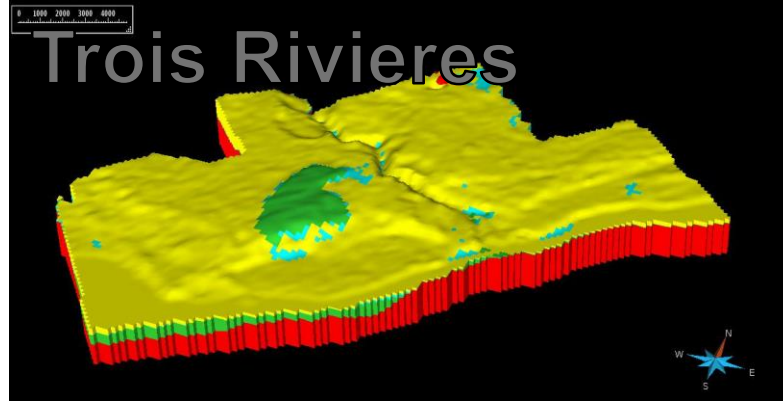
Laval



Mirabel



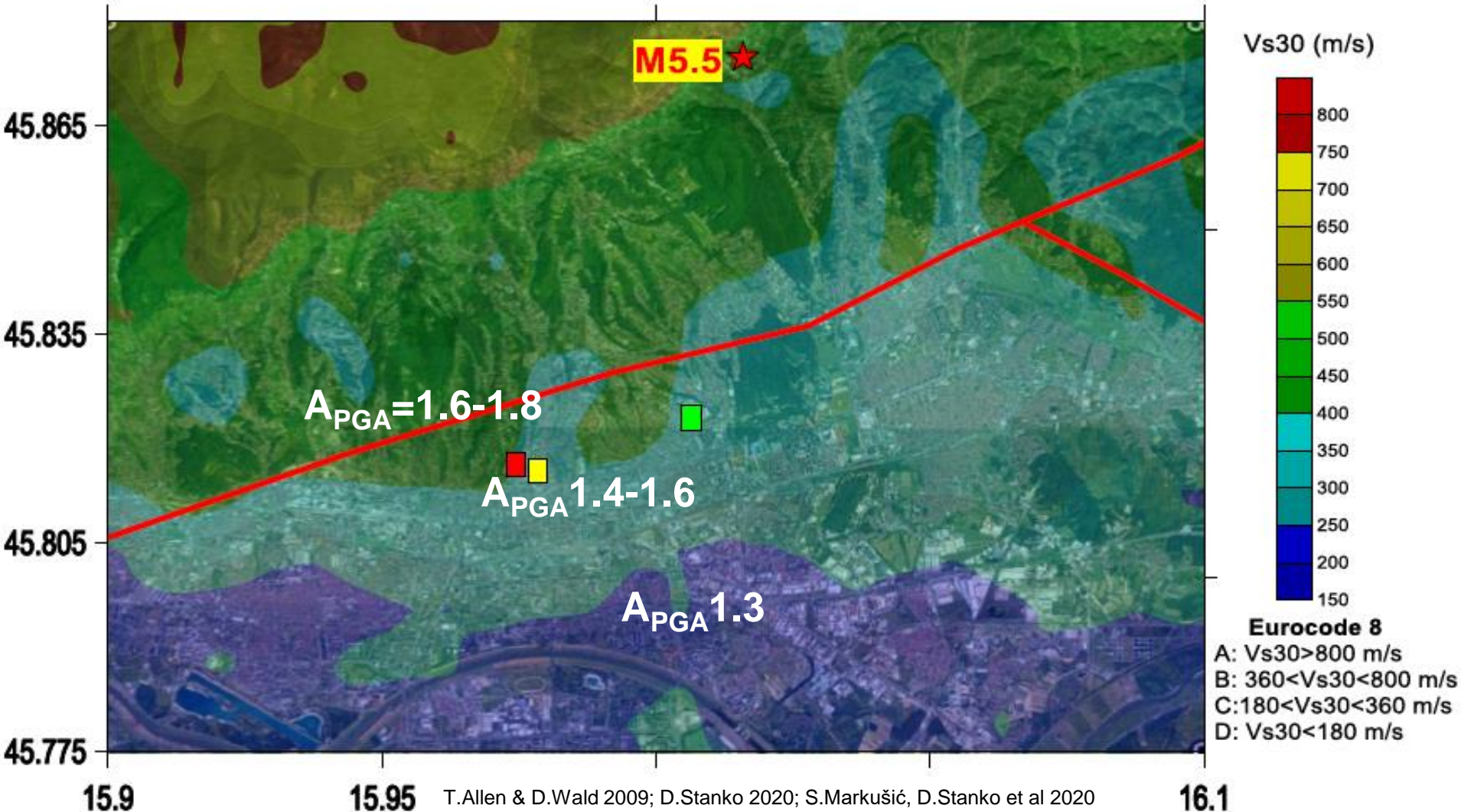
Trois Rivieres



Local site amplification

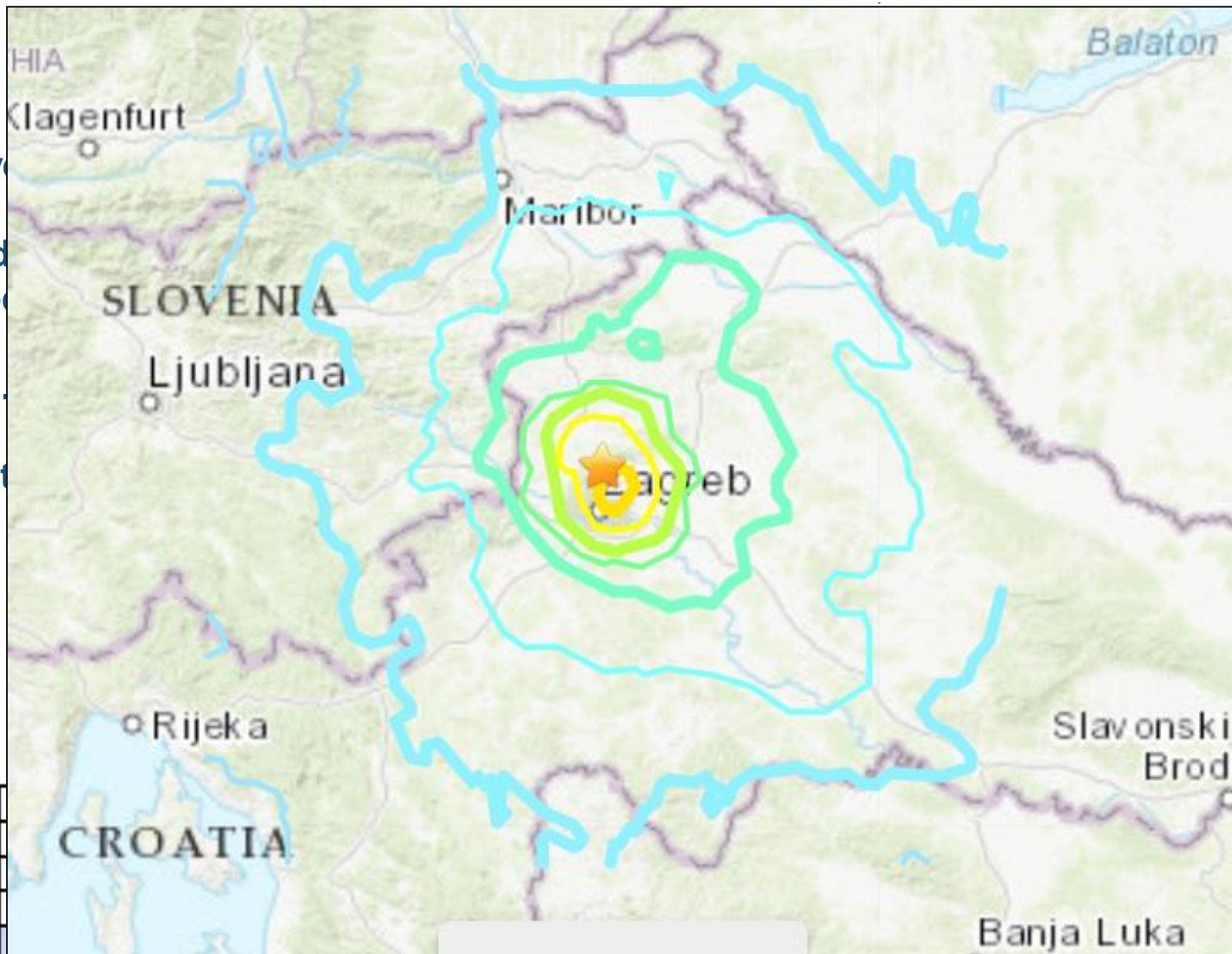
Utjecaj lokalnih uvjeta tla (V_{s30} - topografija)

Ulazno potresno gibanje $PGA=0.185g$

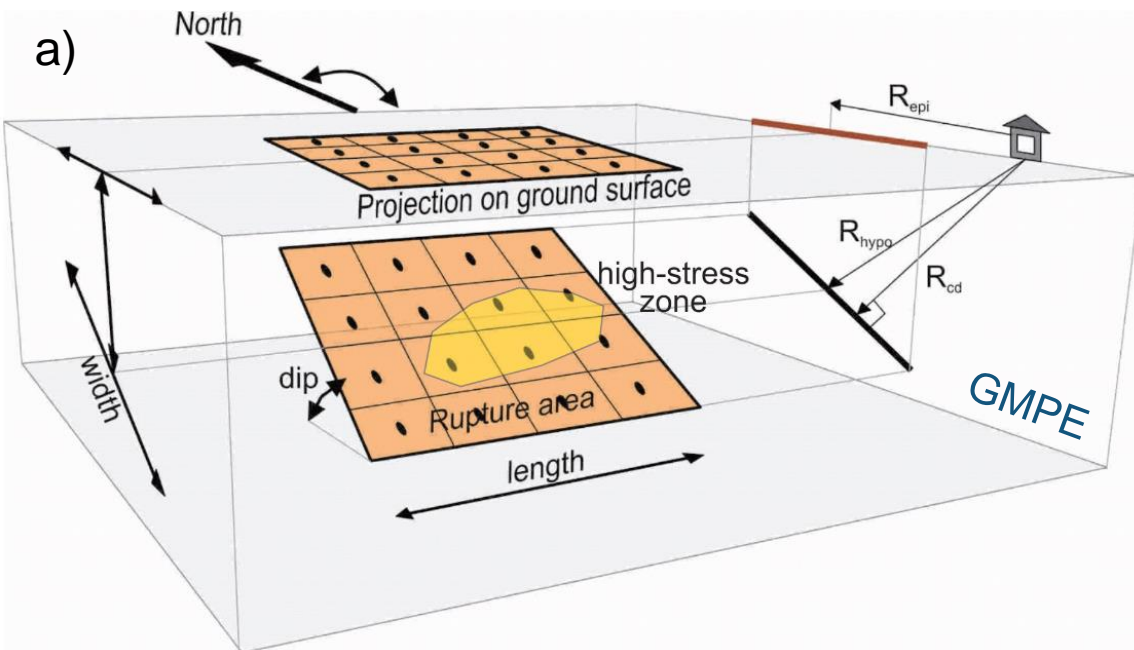


USGS shakemap: March 22, 2020 M_L5.5 Zagreb

- Perceived strong – v
- Potential d
light – mo
- PGA (g): 0.
- Instrument



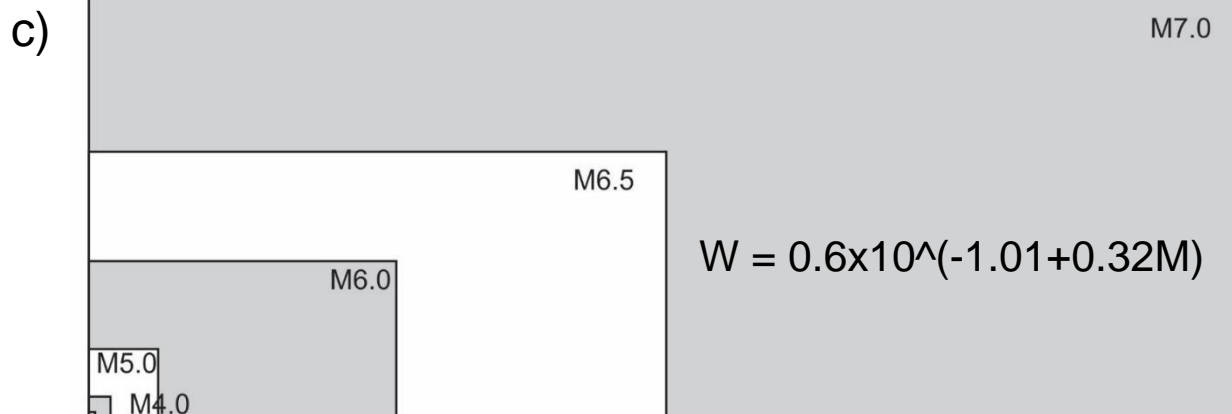
Event scenario modelling (point source vs. FF)



Rupture length:

- 2004 M9.2 Sumatra - 1000 km
- 2011 M9.0 Tohoku - 500 km
- 2010 M7.0 Haiti - 40 km
- 1988 M5.9 Saguenay - 10 km
- 2010 M5.0 Val-des-Bois - 1 km

Top depth = 21-2.5M



$$L = 0.6 \times 10^{(-2.44 + 0.59M)}$$

- disaster planning
- preparedness exercises
- emergency response
- post-eq. recovery
- public/sci. info

Deaggregation of Seismic Hazard

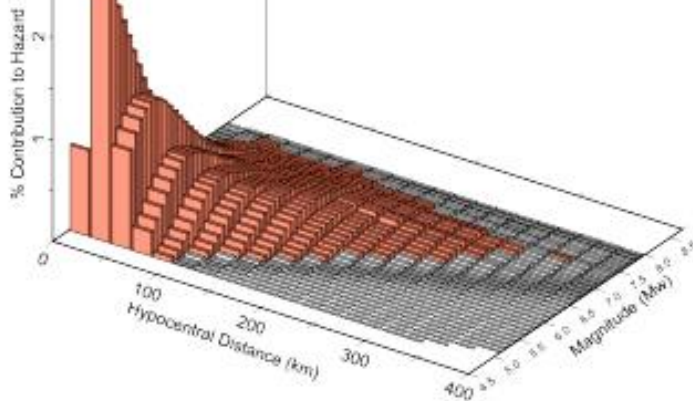
Identifying predominant sources

Montréal

40%/50 year probability, PGA

Probability 0.010 per annum, seismic hazard = 0.037 g
 Mean magnitude (Mw) 5.98 Mean distance 87 km
 Mode magnitude (Mw) 4.85 Mode distance 30 km

P=1/100y, Mw=5.98, D=87km

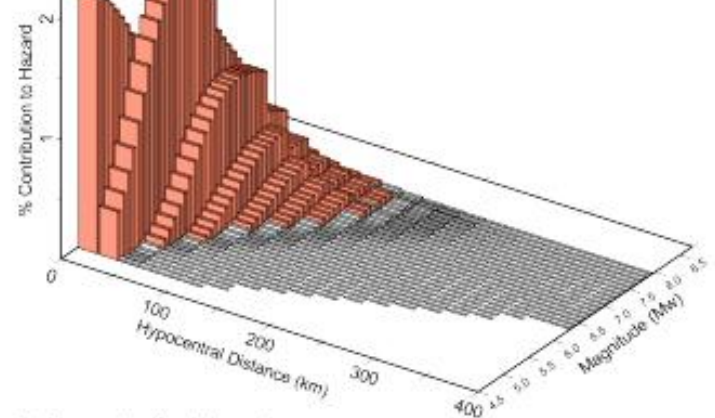


Montréal

5%/50 year probability, PGA

Probability 0.0010 per annum, seismic hazard = 0.217 g
 Mean magnitude (Mw) 6.28 Mean distance 37 km
 Mode magnitude (Mw) 4.85 Mode distance 10 km

P=1/1000y, Mw=6.28, D=37km

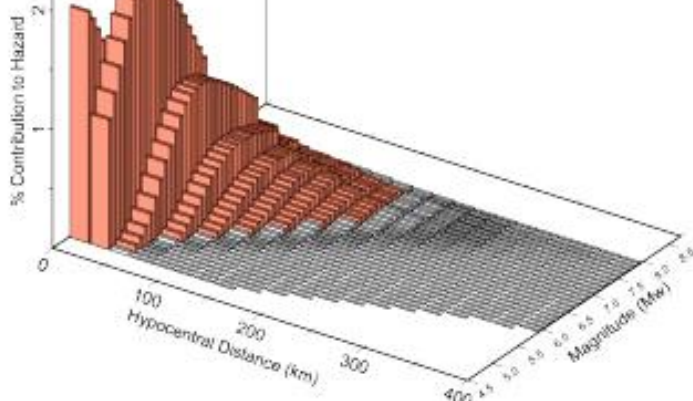


Montréal

10%/50 year probability, PGA

Probability 0.0021 per annum, seismic hazard = 0.131 g
 Mean magnitude (Mw) 6.17 Mean distance 46 km
 Mode magnitude (Mw) 5.55 Mode distance 30 km

P=1/475y, Mw=6.17, D=46km

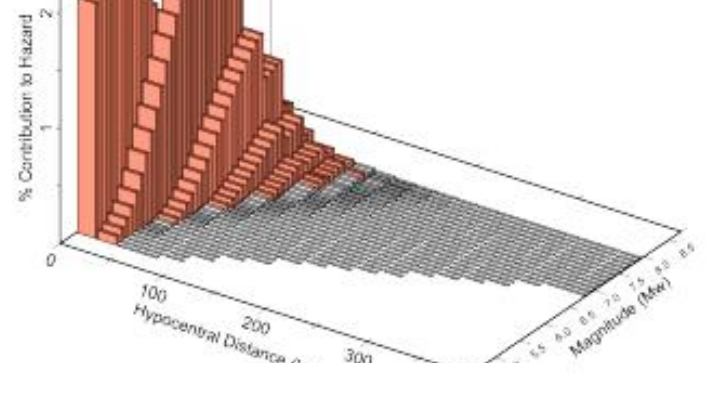


Montréal

2%/50 year probability, PGA

Probability = 0.000404 p.a., Seismic hazard = 0.374 g
 Mean magnitude (Mw) 6.42 Mean distance 29 km
 Mode magnitude (Mw) 6.75 Mode distance 30 km

P=1/2500y, Mw=6.42, D=29km



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Standardized inventory (buildings)

No.	Label	Description	Height			
			Range		Typical	
			Name	Stories	Stories	Feet
1	W1	Wood, Light Frame ($\leq 5,000$ sq. ft.)		1 - 2	1	14
2	W2	Wood, Commercial and Industrial ($> 5,000$ sq. ft.)		All	2	24
3	S1L	Steel Moment Frame	Low-Rise	1 - 3	2	24
4	S1M		Mid-Rise	4 - 7	5	60
5	S1H		High-Rise	8+	13	156
6	S2L	Steel Braced Frame	Low-Rise	1 - 3	2	24
7	S2M		Mid-Rise	4 - 7	5	60
8	S2H		High-Rise	8+	13	156
9	S3	Steel Light Frame		All	1	15
10	S4L	Steel Frame with Cast-in-Place Concrete Shear Walls	Low-Rise	1 - 3	2	24
11	S4M		Mid-Rise	4 - 7	5	60
12	S4H		High-Rise	8+	13	156
13	S5L	Steel Frame with Unreinforced Masonry Infill Walls	Low-Rise	1 - 3	2	24
14	S5M		Mid-Rise	4 - 7	5	60
15	S5H		High-Rise	8+	13	156
16	C1L	Concrete Moment Frame	Low-Rise	1 - 3	2	20
17	C1M		Mid-Rise	4 - 7	5	50
18	C1H		High-Rise	8+	12	120
19	C2L	Concrete Shear Walls	Low-Rise	1 - 3	2	20
20	C2M		Mid-Rise	4 - 7	5	50
21	C2H		High-Rise	8+	12	120
22	C3L	Concrete Frame with Unreinforced Masonry Infill Walls	Low-Rise	1 - 3	2	20
23	C3M		Mid-Rise	4 - 7	5	50
24	C3H		High-Rise	8+	12	120
25	PC1	Precast Concrete Tilt-Up Walls		All	1	15
26	PC2L	Precast Concrete Frames with Concrete Shear Walls	Low-Rise	1 - 3	2	20
27	PC2M		Mid-Rise	4 - 7	5	50
28	PC2H		High-Rise	8+	12	120
29	RM1L	Reinforced Masonry Bearing Walls with Wood or Metal Deck Diaphragms	Low-Rise	1-3	2	20
30	RM2M		Mid-Rise	4+	5	50
31	RM2L	Reinforced Masonry Bearing Walls with Precast Concrete Diaphragms	Low-Rise	1 - 3	2	20
32	RM2M		Mid-Rise	4 - 7	5	50
33	RM2H		High-Rise	8+	12	120
34	URML	Unreinforced Masonry Bearing Walls	Low-Rise	1 - 2	1	15
35	URM M		Mid-Rise	3+	3	35
36	MH	Mobile Homes		All	1	10

Design level

- pre-code
- low-code
- med-code
- high code

Occupancy class

- residential
- commercial
- industrial
- agriculture
- religion
- government
- education

#1: W1

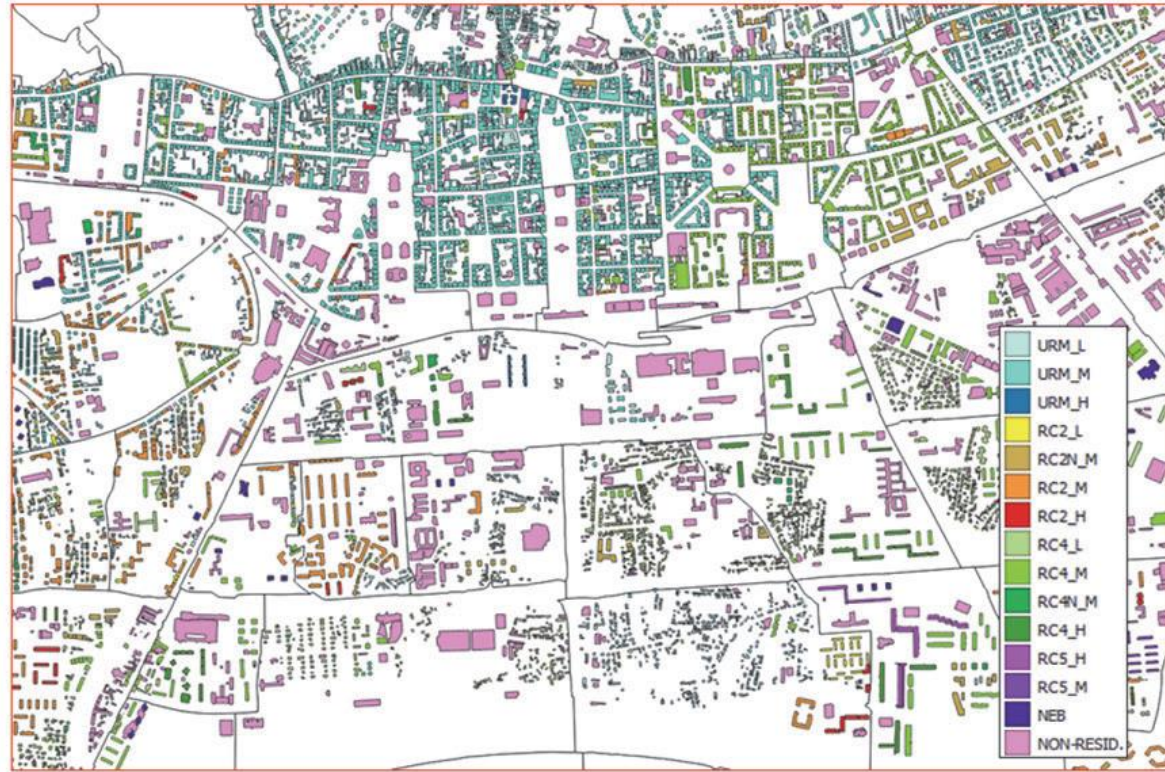
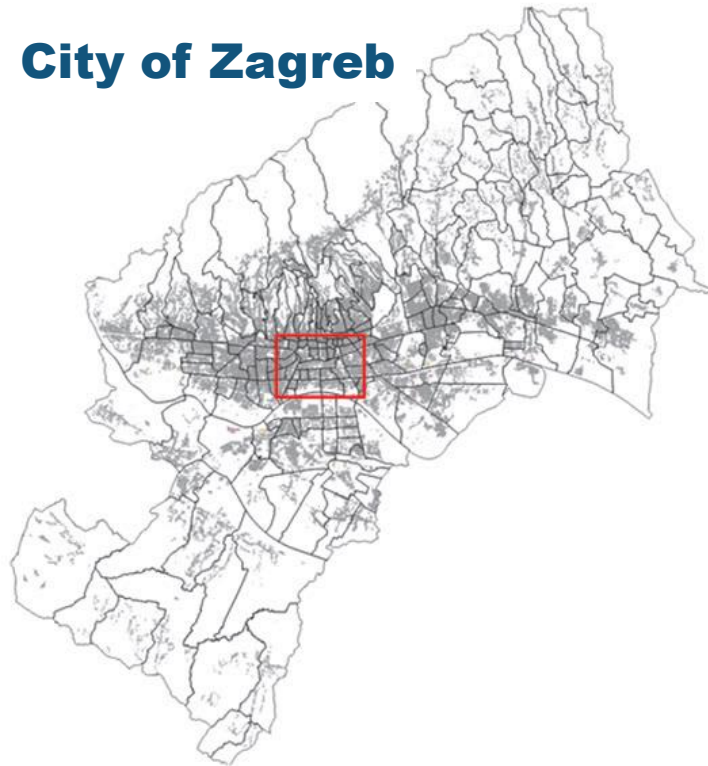
- Wood light frame (< 460 m²)
- Low-Rise: 1-2 Stories
- Residential occupancy

#20: C2M

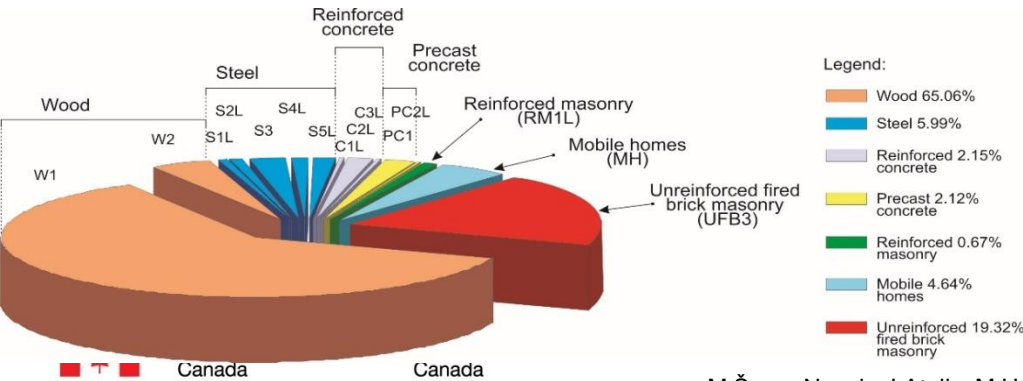
- Concrete Shear Walls
- Mid-Rise: 4-7 Stories
- Education

Aggregated vs. Individual Inventory Data

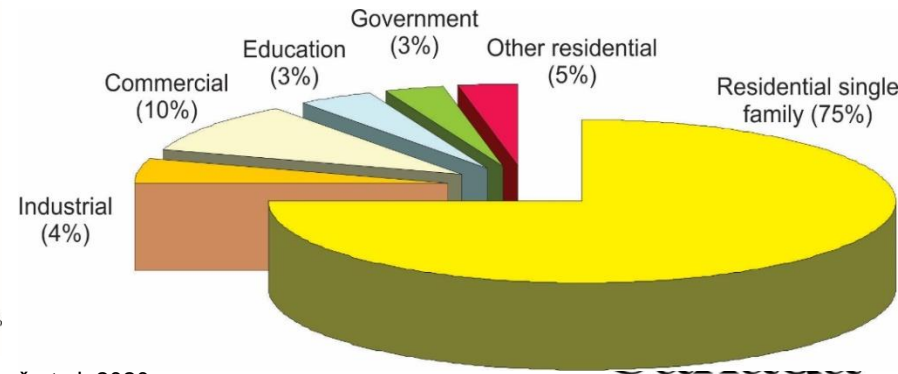
City of Zagreb



Structural types

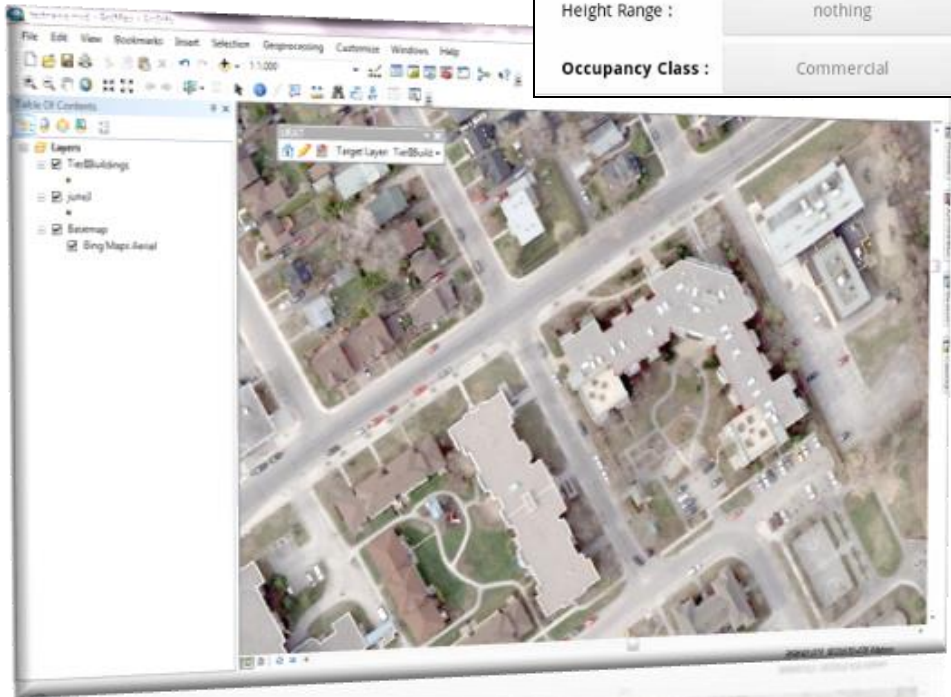


Occupancy types



Exposure: Urban Field RAT app

Building Form	
<input type="button" value="New Building"/>	<input type="button" value="Choose"/>
Building ID : new	
Building Type :	Wood, Commercial and Industrial
# Stories :	3
Height Range :	nothing
Occupancy Class :	Commercial

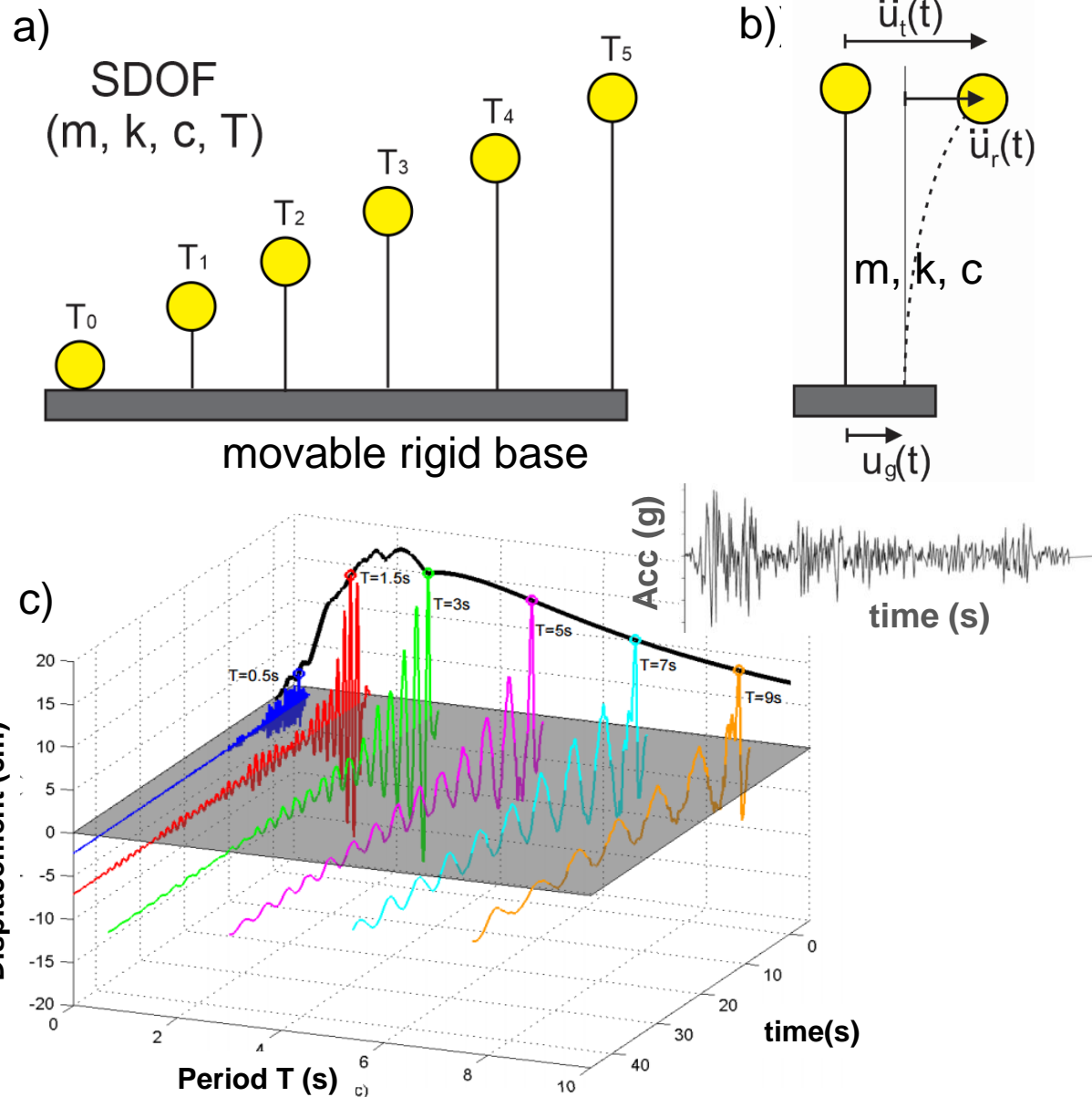


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Earthquake Response Spectrum



Equation of motion:

$$F_{\text{inertia}} + F_{\text{damping}} + F_{\text{elastic}} = 0$$

$$m\ddot{u}_g(t) = m\ddot{u}_r(t) + c\dot{u}_r + ku_r$$

$$m\ddot{u}_t(t) = c\dot{u}_r + ku_r$$

c : coeff. viscous damping
(% of critical damping)

k : stiffness = $m\omega^2$, $\omega = 2\pi/T$

ω : natural (angular) frequency

Elastic response:

Spectral (pseudo) acceleration:

$$S_a(t) = \omega_i^2 u_r(t)$$

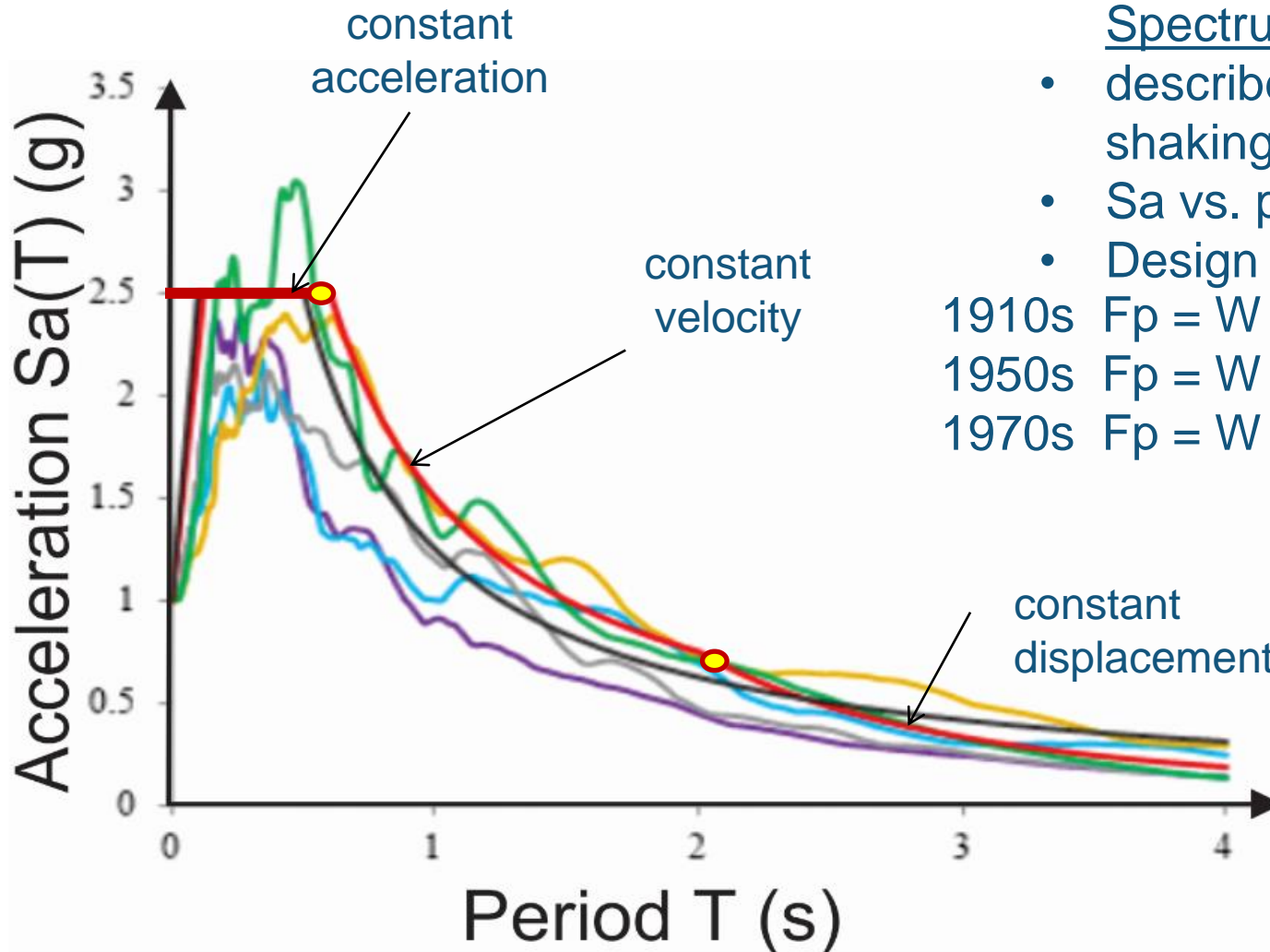
Maximum ground acceleration:

$$PGA = \ddot{u}_g^{\text{max}}(t)$$

Maximum ground velocity:

$$PGV = \max \int \ddot{u}_g(t) dt$$

Response spectrum UHS



- smoothed Elastic Response Spectrum for SDOF
- describes the design ground shaking
- S_a vs. period T domain
- Design codes (base shear)

1910s $F_p = W \times 0.1$

1950s $F_p = W \times S_a(T_o)$

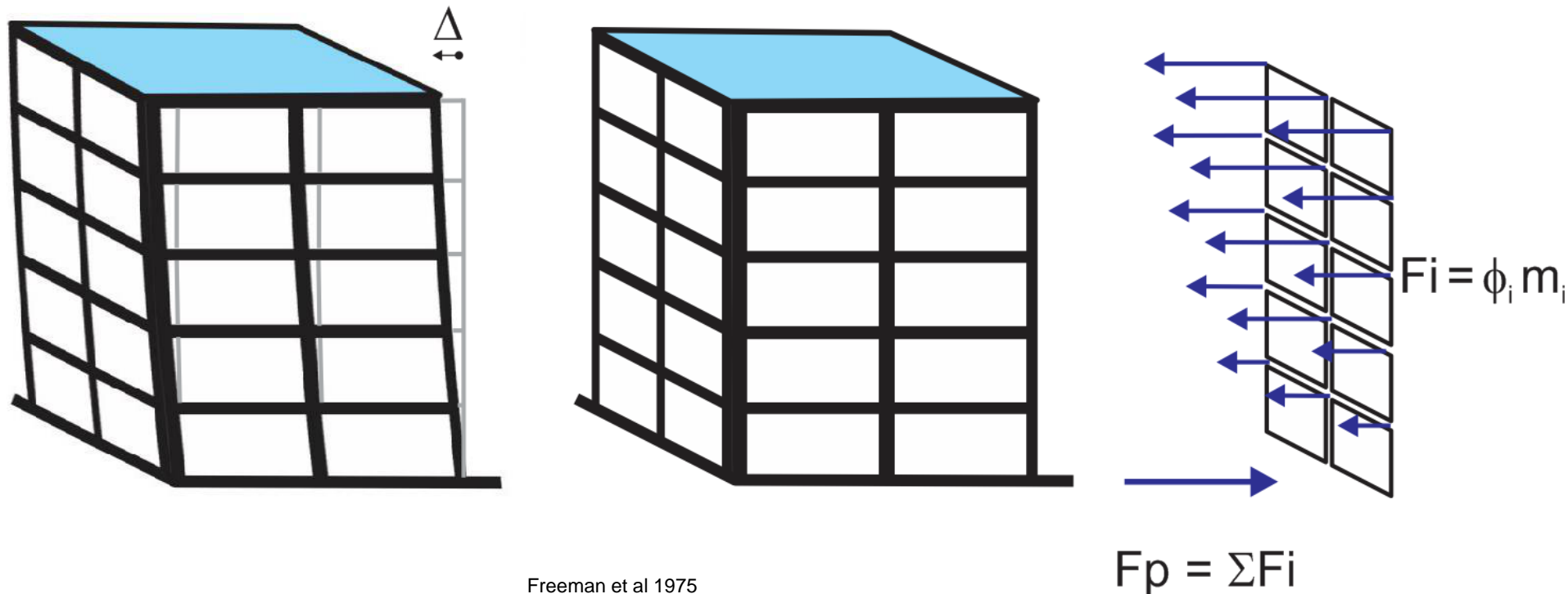
1970s $F_p = W \times S_a(T_o) \times \text{Factors}$



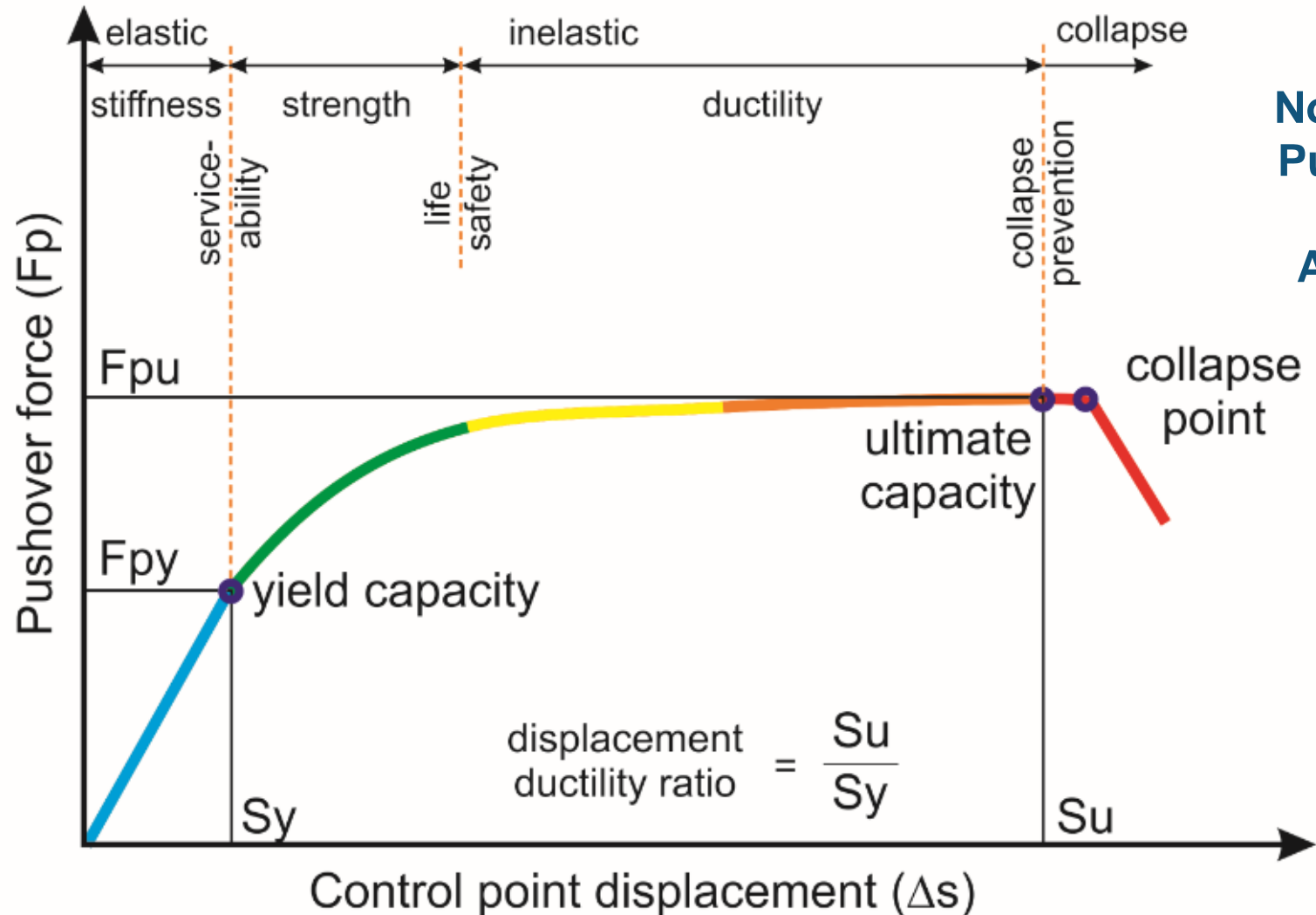
Seismic vulnerability: capacity curve

- Static Nonlinear Pushover Based Analysis vs. NRHA
- Choose height-wise distribution of lateral forces
- Monotonically increase lateral forces
- Develop capacity (pushover) curve as base shear vs. lateral deformation

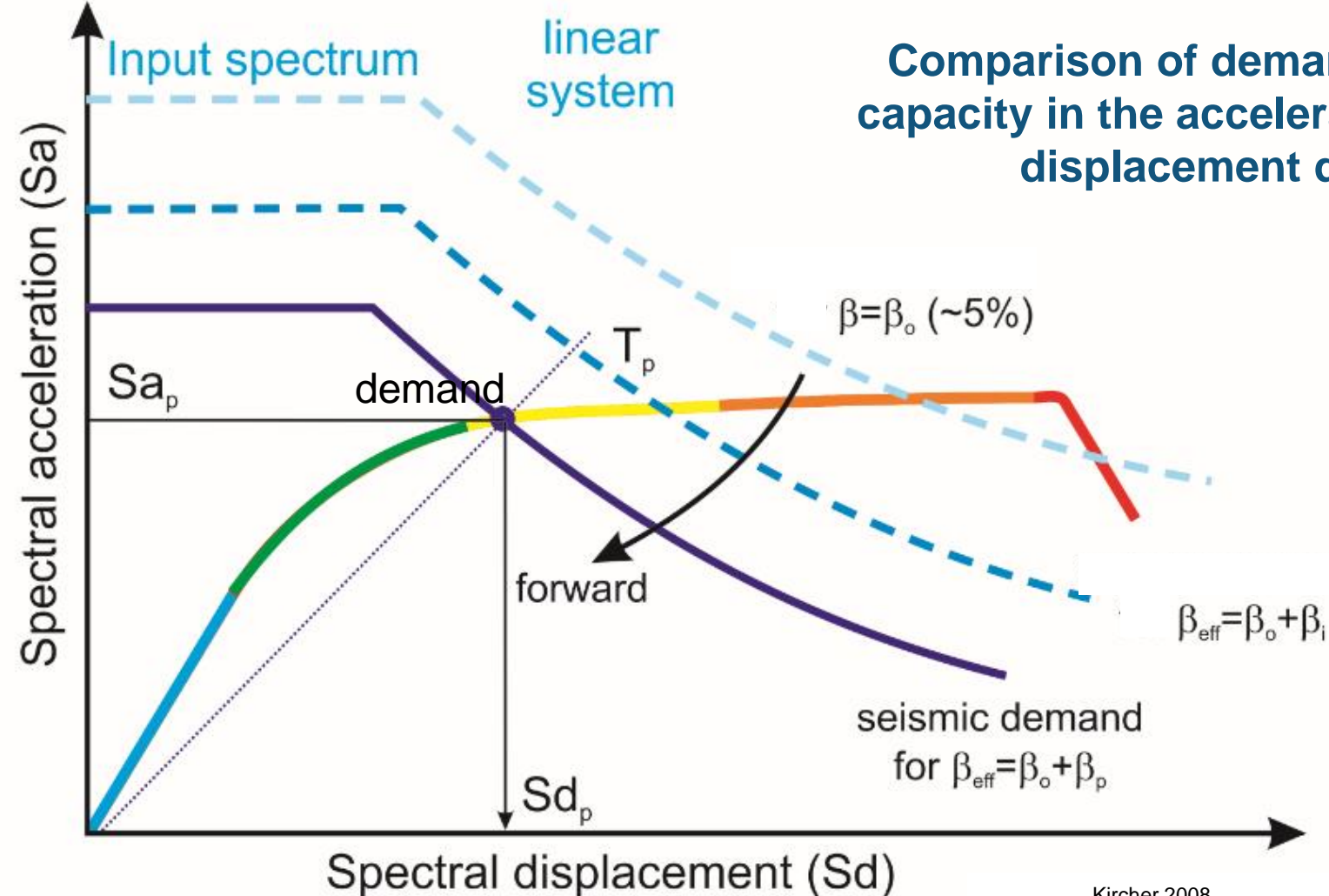
Control point displacement (roof displacement, IS drift)



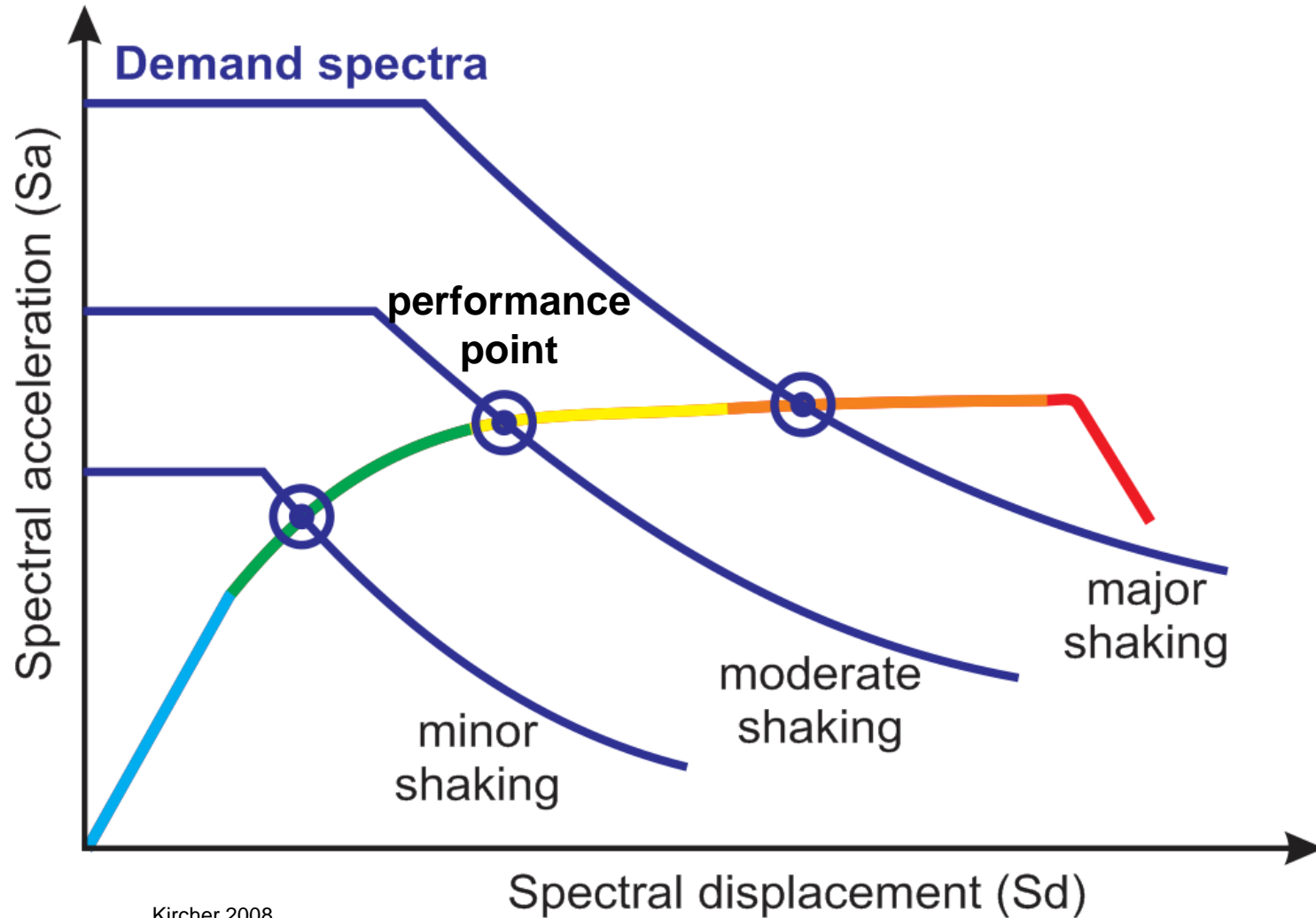
Seismic vulnerability: capacity curve



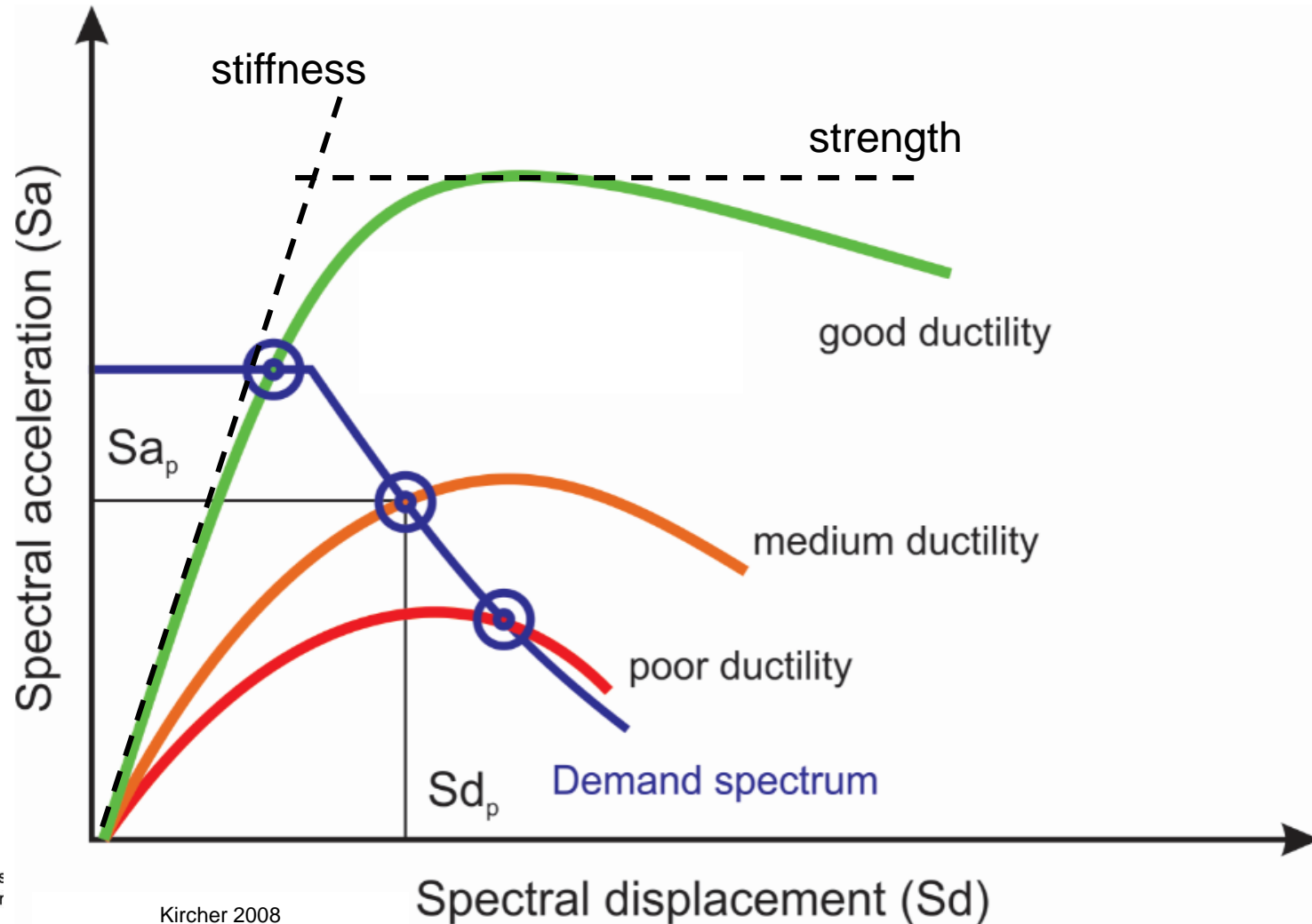
Seismic vulnerability: CSM (Sa vs. Sd domain)



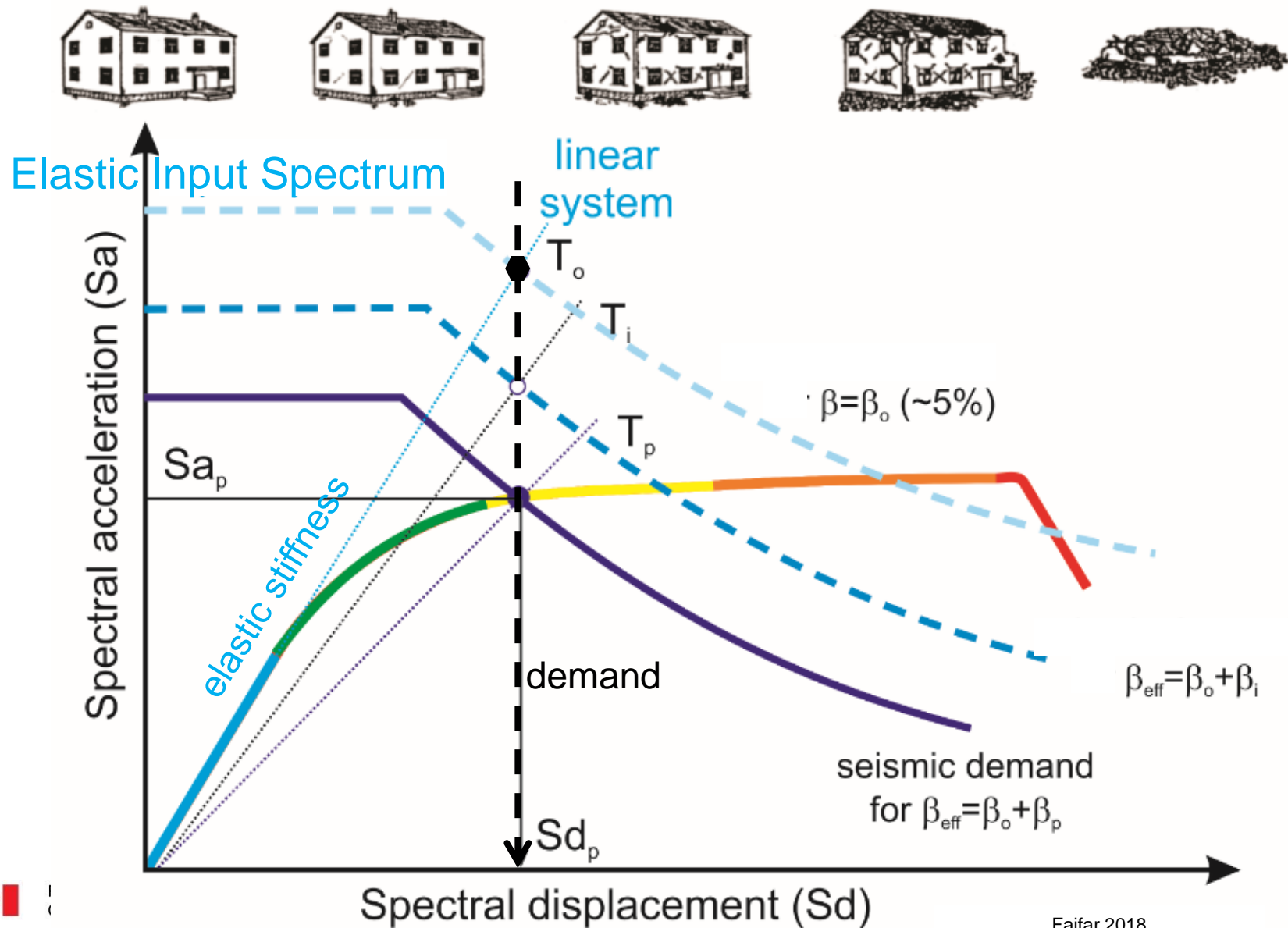
Seismic vulnerability: CSM



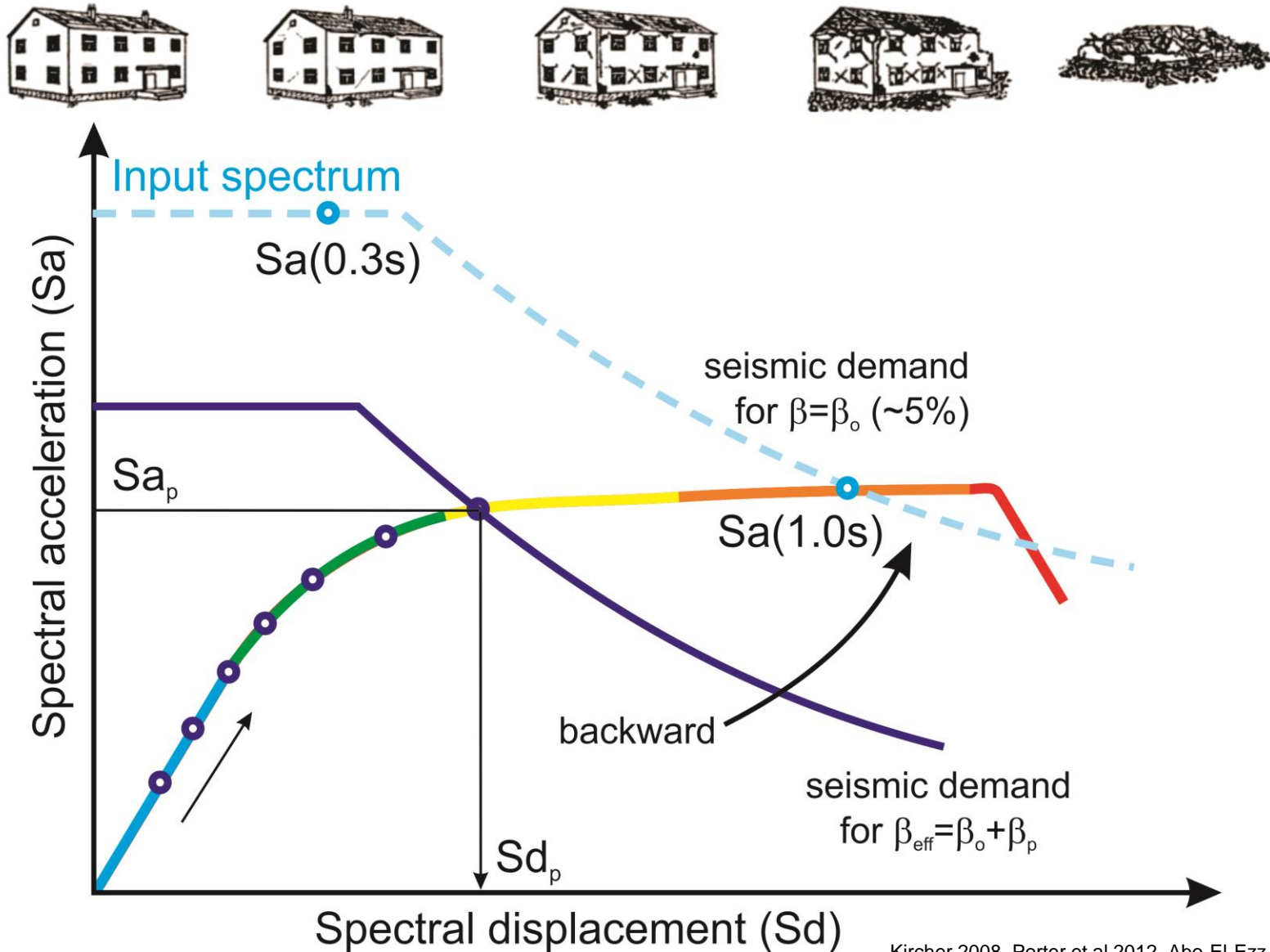
Seismic vulnerability: CSM



Seismic vulnerability: CSM



Seismic vulnerability: CSM



Seismic vulnerability: damage curves

Analytical method



No damage (DS0)



Slight damage (DS1):
First wall Flexural cracking



Moderate damage (DS2):
First wall Shear cracking



Extensive damage (DS3):
Maximum base shear capacity of the building

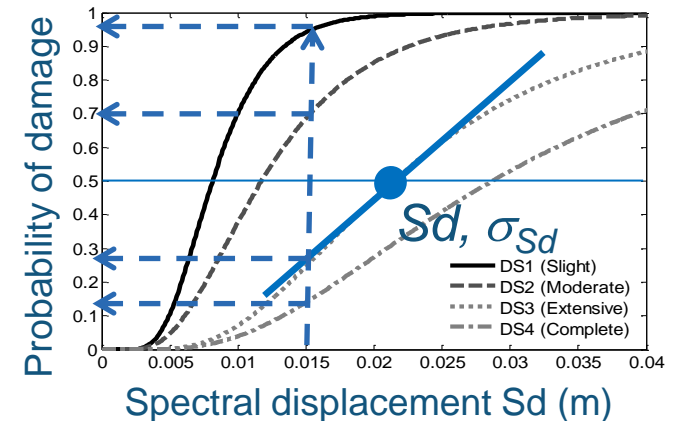


Complete damage (DS4):
20% reduction in base shear capacity

Fragility data:

Median values S_d

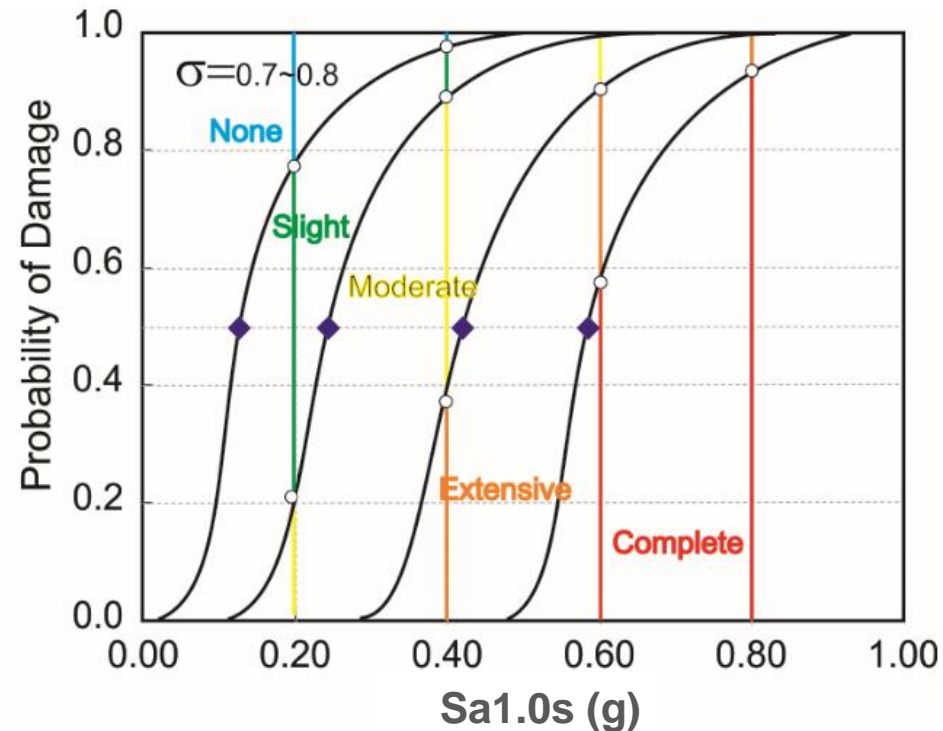
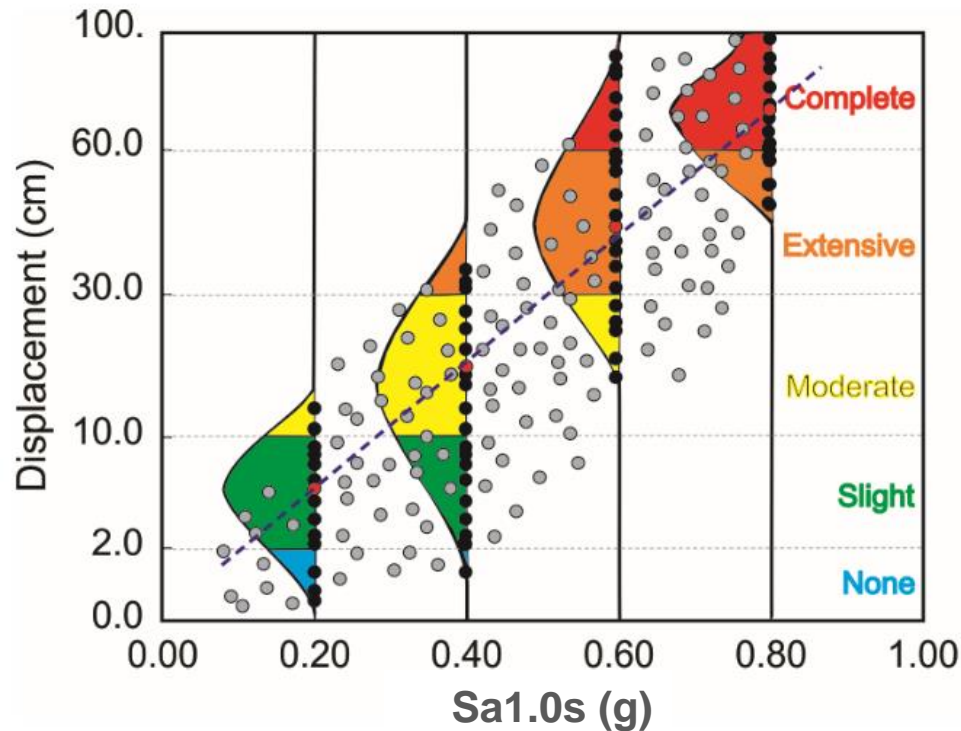
Standard deviations σ_{S_d}



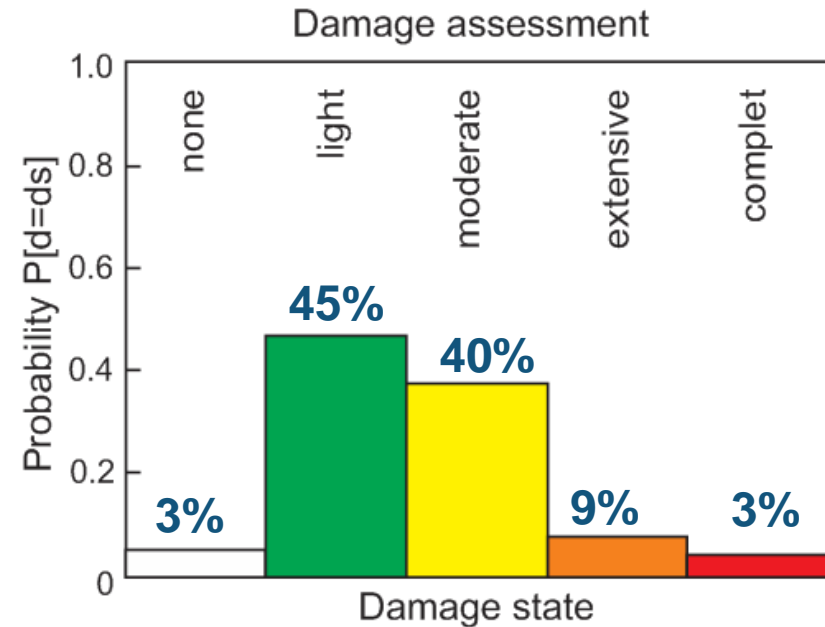
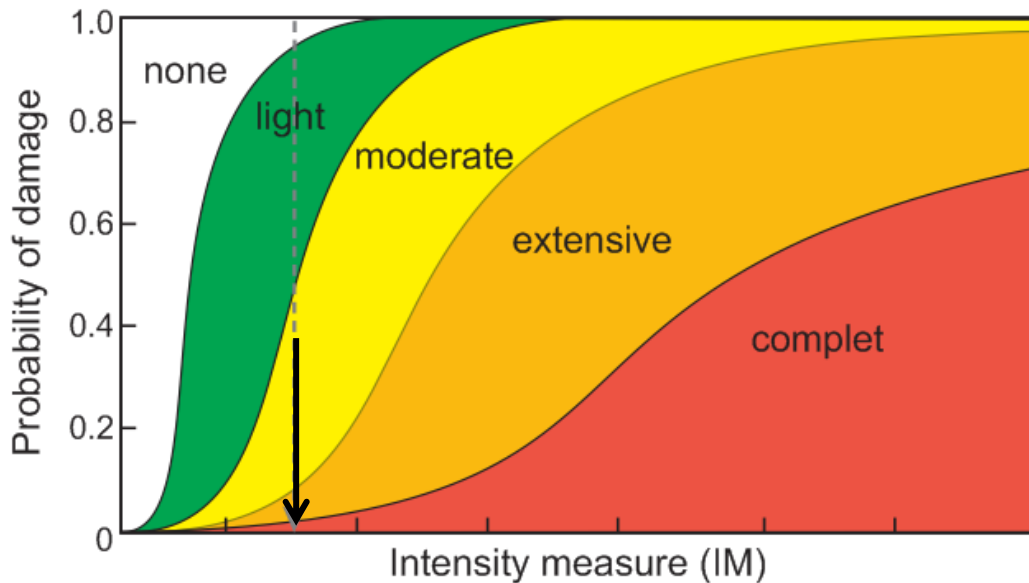
Damage state DS	ISD [%]
Slight	0.05
Moderate	0.8
Extensive	1.15
Complete	2.8

Seismic vulnerability: damage curves

Empirical based on post-earthquake damage observations
 $S_a(1.0)$ used as IMs of seismic shaking



Seismic vulnerability: damage curves

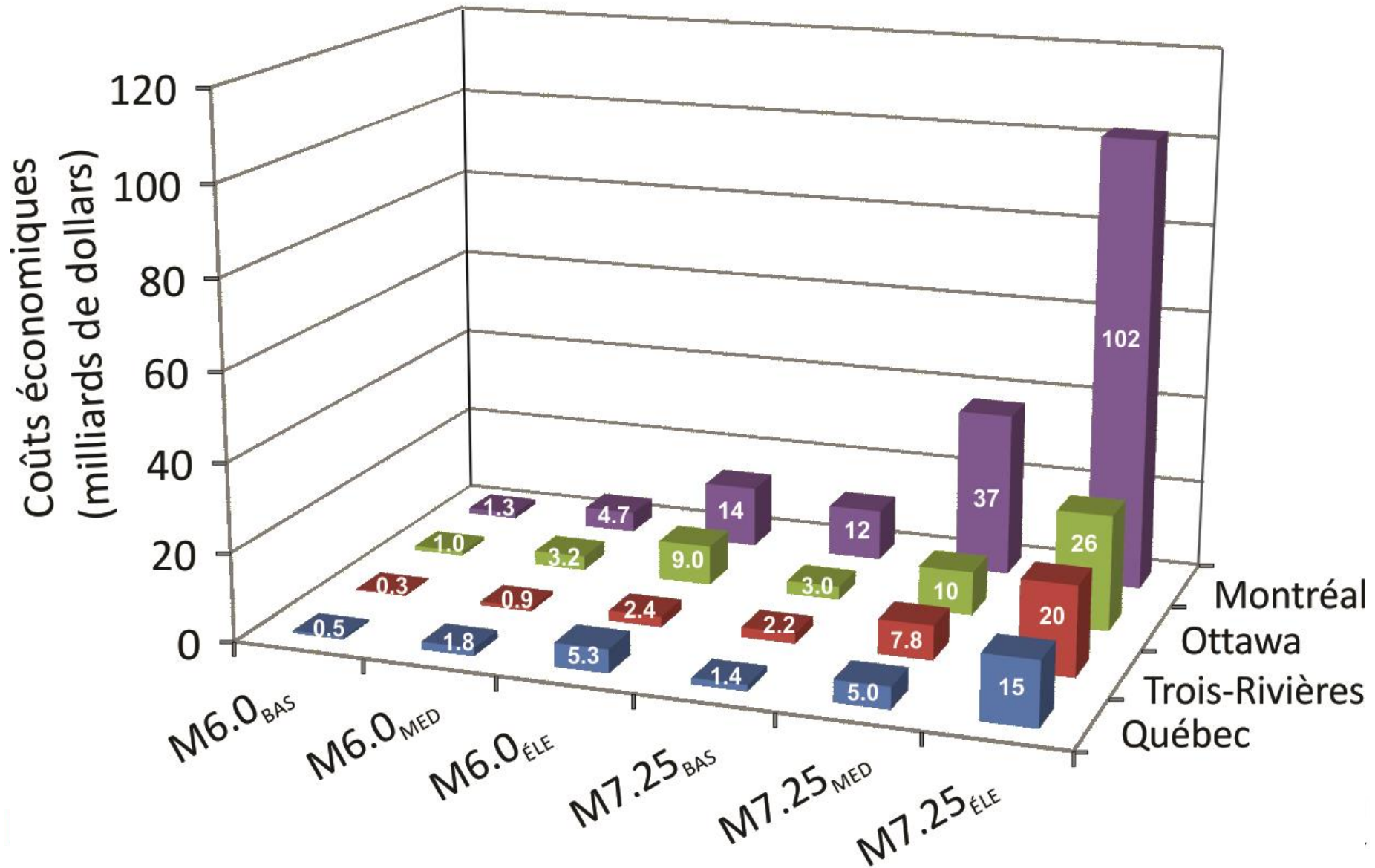


Damage factors: cost of repair - % replacement cost (example 100,000€)

	none	light	mod.	ext.	compl.	
Turkey	0%	5%	30%	70%	100%	$\Sigma=0+2,250+12,000+6,300+3,000=$
USA	0%	2%	10%	50%	100%	$\Sigma=0+ 900+ 4,000+4,500+3,000=$
						23,550€
						12,400€



Uncertainty analysis



Risk communication - ER2

- Despite numerous research efforts in recent years, seismic risk continues to be difficult to perceive and communicate
 - **Risk assessment**
 - **Risk communication**
 - Risk perception
 - Risk management
- ER2 Rapid Risk Evaluator
 - <https://er2.geosciences.ca/earthquake>
 - username: MNastev
 - password: NjE8ZePM
 - https://www.youtube.com/watch?v=kNZbv0VPsmw&feature=youtu.be&ab_channel=NickGibb

